

Seismic Analysis of Multi-Storey Building with Plus Shape RC Shear Walls at The Center in Concrete Frame Structure With Different Type of Soil Condition

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ABSTRACT: Shear walls provide large strength and stiffness to buildings in the direction of their orientation, which significantly reduces lateral sway of the building and thereby reduces damage to structure and its contents. Shear walls should be provided along preferably both length and width. Shear walls are analyzed to resist two types of forces: shear forces and uplift forces. Shear forces are created throughout the height of the wall between the top and bottom shear wall connections. Uplift forces exist on shear walls because the horizontal forces are applied to the top of the wall. These uplift forces try to lift up one end of the wall and push the other end down. In some cases, the uplift force is large enough to tip the wall over. The seismic motion that reaches a structure on the surface of the earth is influenced by local soil conditions. The subsurface soil layers underlying the building foundation may amplify the response of the building to earthquake motions originating in the bedrock. Three types soil are considered here: Hard soil, Medium soil, soft soil. In this study 30 story building with plus (+) Shape RC Shear wall at the center in Concrete Frame Structure with fixed support conditions under different type of soil for earthquake zone V as per IS 1893 (part 1) : 2002 in India are analyzed using software ETABS by Dynamic analysis (Response Spectrum method). All the analyses has been carried out as per the Indian Standard code books. This paper aims to Study the behaviour of high rise structure with dual system with Plus Shape RC Shear Walls under different type of soil condition with seismic loading. Estimation of structural response such as; stiffness, lateral loads, storey displacements, storey moment, storey shear, storey drift, Pier Forces, column forces and Mode shapes of shear wall is carried out.

Keywords: Response Spectrum method, Soft, Medium & Hard Soil, Structural Response, Plus Shape Shear Wall, ETABS software

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I. INTRODUCTION

1.1 Background

Shear walls in high seismic regions require special detailing. However, in past earthquakes, even buildings with sufficient amount of walls that were not specially detailed for seismic performance (but had enough well-distributed reinforcement) were saved from collapse. Shear walls are efficient, both in terms of construction cost and effectiveness in minimizing earthquake damage in structural and nonstructural elements (like glass windows and building contents). Shear walls provide large strength and stiffness to buildings in the direction of their orientation, which significantly reduces lateral sway of the building and thereby reduces damage to structure and its contents. Shear walls should be provided along preferably both length and width. Shear walls in buildings must be symmetrically located in plan to reduce ill-effects of twist in buildings. They could be placed symmetrically along one or both directions in plan. Buildings are designed primarily to serve the needs of an intended occupancy. One of the dominant design requirements is therefore the provision of an appropriate internal layout of buildings. Once the functional layout is established, one must develop a structural system that will satisfy the established design criteria as efficiently and economically as possible, while fitting into the architectural layout. The vital structural criteria are an adequate reserve of strength against failure, adequate lateral stiffness and an efficient performance during the service life of the buildings. In modern tall buildings, shear walls are commonly used as a vertical structural element for resisting the lateral loads that may be induced by the effect of wind and earthquakes. Shear walls of varying cross sections i.e. rectangular shapes to

more irregular cores such as channel, T, L, barbell shape, box etc. can be used. Provision of walls helps to divide an enclosed space, whereas of cores to contain and convey services such as elevator.

1.2 Literature Review

Prajapati R.J. et al., (2013) carried out study on deflection in high rise buildings for different position of shear walls. It was observed that deflection for building with shear walls provided at the corners in both the directions was drastically less when compared with other models. Chandurkar P.P. et al., (2013) conducted a study on seismic analysis of RCC building with and without shear walls. They have selected a ten storied building located in zone II, zone III, zone IV and zone V. Parameters like Lateral displacement, story drift and total cost required for ground floor were calculated in both the cases. Bhat S.M. et al., (2013) carried out study on Earthquake behaviour of buildings with and without shear walls. Parameters like Lateral displacement, story drift etc were found and compared with the bare frame model. Sardar S.J. et al., (2013) studied lateral displacement and inter-story drift on a square symmetric structure with walls at the centre and at the edges, and found that the presence of shear wall can affect the seismic behaviour of frame structure to large extent, and the shear wall increases the strength and stiffness of the structure.

Sagar K. et al., (2012) carried out linear dynamic analysis on two sixteen storey high buildings. It was concluded that shear walls are one of the most effective building elements in resisting lateral forces during earthquake. Providing shear walls in proper position minimizes effect and damages due to earthquake and winds.

Kumbhare P.S. et al., (2012) carried out a study on shear wall frame interaction systems and member forces. It was found that shear wall frame interaction systems are very effective in resisting lateral forces induced by earthquake. Placing shear wall away from center of gravity resulted in increase in the most of the members forces. It follows that shear walls should be coinciding with the centroid of the building. Rahman A. et al., (2012) studied on drift analysis due to earthquake load on tall structures. In this study regular shaped structures have been considered. Estimation of drift was carried out for rigid frame structure, coupled shear wall structure and wall frame structure.

Anshuman et al., (2011) conducted a research on solution of shear wall location in multi storey building. An earthquake load was calculated and applied to a fifteen storied building located in zone IV. It was observed that the top deflection was reduced and reached within the permissible deflection after providing the shear wall. Kameshwari B. et al., (2011) analyzed the effect of various configurations of shear walls on high-rise structure. The drift and inter-storey drift of the structure in the following configurations of shear wall panels was studied and was compared with that of bare frame. Diagonal shear wall configuration was found to be effective for structures in the earthquake prone areas.

Based on the literature review, the salient objective of the present study have been identified as follows:

- ❖ behaviour of high rise structure with dual system with Plus shape RC Shear Walls with seismic loading.
- ❖ To examine the effect of different types of soil (Hard, medium and Soft) on the overall interactive behaviour of the shear wall foundation soil system.
- ❖ The variation of maximum storey shear, storey moment of the models has been studied.
- ❖ The variation of storey drifts of the models has been studied
- ❖ The variation of displacement of the models has been studied
- ❖ The variation of Time period and frequency has been studied.
- ❖ The variation of maximum column axial force, maximum column shear force, maximum column moment and maximum column torsion of the model have been studied.
- ❖ The variation of Pier axial force, Pier shear force, Pier moment and Pier torsion of the models have been studied.

1.3 Shear Wall Structure

The usefulness of shear walls in framing of buildings has long been recognized. Walls situated in advantageous positions in a building can form an efficient lateral-force-resisting system, simultaneously fulfilling other functional requirements. When a permanent and similar subdivision of floor areas in all stories is required as in the case of hotels or apartment buildings, numerous shear walls can be utilized not only for lateral force resistance but also to carry gravity loads. In such case, the floor by floor repetitive planning allows the walls to be vertically continuous which may serve simultaneously as excellent acoustic and fire insulators between the apartments. Shear walls may be planar but are often of L-, T-, I-, or U- shaped section to better suit the planning and to increase their flexural stiffness. The positions of shear walls within a building are usually dictated by functional requirements. These may or may not suit structural planning. The purpose of a building

and consequent allocation of floor space may dictate required arrangements of walls that can often be readily utilized for lateral force resistance. Building sites, architectural interests or client's desire may lead the positions of walls that are undesirable from a structural point of view. However, structural designers are often in the position to advise as to the most desirable locations for shear walls in order to optimize seismic resistance. The major structural considerations for individual shear walls will be aspects of symmetry in stiffness, torsional stability and available overturning capacity of the foundations (Paulay and Priestley, 1992).

1.4 Essentials Of Structural Systems For Seismic Resistance

The primary purpose of all structural members used in buildings is to support gravity loads. However, buildings may also be subjected to lateral forces due to wind and earthquakes. The effects of lateral forces in buildings will be more significant as the building height increases. All structural systems will not behave equally under seismic excitation. Aspects of structural configuration, symmetry, mass distribution and vertical regularity must be considered. In addition to that, the importance of strength, stiffness and ductility in relation to acceptable response must be evaluated in structural system (Paulay and Priestley, 1992).

The first task of the structural designer is to select the appropriate structural system for the satisfactory seismic performance of the building within the constraints dictated by architectural requirements. It is better where possible to discuss architect and structural engineer for alternative structural configuration at the earliest stage of concept development. Thus, undesirable geometry is not locked into the system before structural design is started.

Irregularities in buildings contribute to complexity of structural behavior. When not recognized, they may result in unexpected damage and even collapse of the structures. There are many possible sources of structural irregularities. Drastic changes in geometry, interruptions in load path, discontinuities in both strength and stiffness, disruption in critical region by openings and unusual proportion of members are few of the possibilities. The recognition of many of these irregularities and of conceptions for remedial measures for the mitigation of their undesired effects relies on sound understanding of structural behavior.

II. METHODOLOGY

Earthquake motion causes vibration of the structure leading to inertia forces. Thus a structure must be able to safely transmit the horizontal and the vertical inertia forces generated in the super structure through the foundation to the ground. Hence, for most of the ordinary structures, earthquake-resistant design requires ensuring that the structure has adequate lateral load carrying capacity. Seismic codes will guide a designer to safely design the structure for its intended purpose.

1. Dynamic analysis.
2. Response spectrum method.
3. Time history method.

2.1 Dynamic Analysis

Dynamic analysis shall be performed to obtain the design seismic force, and its distribution in different levels along the height of the building, and in the various lateral load resisting element, for the following buildings:

2.1.1 Regular buildings: Those greater than 40m in height in zones IV and V, those greater than 90m in height in zone II and III.

2.1.2 Irregular buildings: All framed buildings higher than 12m in zones IV and V, and those greater than 40m in height in zones II and III.

The analysis of model for dynamic analysis of buildings with unusual configuration should be such that it adequately models the types of irregularities present in the building configuration. Buildings with plan irregularities, as defined in Table 4 of IS code: 1893-2002 cannot be modeled for dynamic analysis. Dynamic analysis may be performed either by the TIME HISTORY METHOD or by the RESPONSE SPECTRUM METHOD. However in either method, the design base shear V_B shall be compared with a base shear V_B calculated using a fundamental period T_a . When V_B is less than V_B all the response quantities shall be multiplied by V_B / V_B . The values of damping for a building may be taken as 2 and 5 percent of the critical, for the purpose of dynamic analysis of steel and reinforced concrete buildings, respectively.

2.2 Time History Method

The usage of this method shall be on an appropriate ground motion and shall be performed using accepted principles of dynamics. In this method, the mathematical model of the building is subjected to accelerations from earthquake records that represent the expected earthquake at the base of the structure.

2.3 Response Spectrum Method

The word spectrum in engineering conveys the idea that the response of buildings having a broad range of periods is summarized in a single graph. This method shall be performed using the design spectrum specified in code or by a site-specific design spectrum for a structure prepared at a project site. The values of damping for building may be taken as 2 and 5 percent of the critical, for the purposes of dynamic of steel and reinforce concrete buildings, respectively. For most buildings, inelastic response can be expected to occur during a major earthquake, implying that an inelastic analysis is more proper for design. However, in spite of the availability of nonlinear inelastic programs, they are not used in typical design practice because:

- 1- Their proper use requires knowledge of their inner workings and theories. design criteria, and
- 2- Result produced are difficult to interpret and apply to traditional design criteria , and
- 3- The necessary computations are expensive.

Therefore, analysis in practice typically use linear elastic procedures based on the response spectrum method. The response spectrum analysis is the preferred method because it is easier to use.

2.4 Modes to be Considered

The number of modes to be considered in the analysis should be such that the sum of the total modal masses of all modes considered is at least 90% of the total seismic mass and the missing mass correction beyond 33%. If modes with natural frequency beyond 33 Hz are to be considered, modal combination shall be carried out only for modes up to 33 Hz.

2.5 Computation of Dynamic Quantities

Buildings with regular ,or nominally irregular plan configuration may be modeled as a system of masses lumped at the floor levels with each mass having one degree of freedom, that of lateral displacement in the direction of consideration

2.6 Response Analysis of MDOF System

Multi degree of freedom (MDOF) systems are usually analyzed using Modal Analysis. This system when subjected to ground motion undergoes deformations in number of possible ways. These deformed shapes are known as modes of vibration or mode shapes. Each shape is vibrating with a particular natural frequency. Total unique modes for each MDOF system are equal to the possible degree of freedom of system.

2.7 Design Of Earthquake Resistant Structure Based On Codal Provisions

General principles and design philosophy for design of earthquake-resistant structure are as follows:

- a) The characteristics of seismic ground vibrations at any location depends upon the magnitude of earth quake, its depth of focus, distance from epicenter, characteristic of the path through which the waves travel, and the soil strata on which the structure stands. Ground motions are predominant in horizontal direction.
- b) Earthquake generated vertical forces, if significant, as in large spans where differential settlement is not allowed, must be considered.
- c) The response of a structure to the ground motions is a function of the nature of foundation soil, materials size and mode of construction of structures, and the duration and characteristic of ground motion.
- d) The design approach is to ensure that structures possess at least a minimum strength to withstand minor earthquake (DBE), which occur frequently, without damage; resist moderate earthquake without significant damage though some nonstructural damage may occur, and aims that structures withstand major earthquake (MCE) without collapse. Actual forces that appeared on structures are much greater then the design forces specified here, but ductility, arising due to inelastic material behavior and detailing, and over strength, arising from the additional reserve strength in structures over and above the design strength are relied upon to account for this difference in actual and design lateral forces.
- e) Reinforced and pre-stressed members shall be suitably designed to ensure that premature failure due to shear or bond does not occur, as per IS:456 and IS:1343.
- f) In steel structures, members and their connections should be so proportioned that high ductility is obtained.
- g) The soil structure interaction refers to the effect of the supporting foundation medium on the motion of structure. The structure interaction may not be considered in the seismic analysis for structures supporting on the rocks.
- h) The design lateral forces shall be considered in two orthogonal horizontal directions of the structures. For structures, which have lateral force resisting elements in two orthogonal directions only, design lateral force must be considered in one direction at a time. Structures having lateral resisting elements in two directions other than orthogonal shall be analyzed according to clause 2.3.2 IS 1893 (part 1) : 2002. Where both horizontal and vertical forces are taken into account, load combinations must be according to clause 2.3.3 IS

1893 (part 1) : 2002.

- i) When a change in occupancy results in a structure being re-classified to a higher importance factor (I), the structure shall be confirm to the seismic requirements of the new structure with high importance factor.

III . MODELING OF BUILDING

3.1 Details of The Building

A symmetrical building of plan 38.5m X 35.5m located with location in zone V, India is considered. Four bays of length 7.5m& one bays of length 8.5m along X - direction and Four bays of length 7.5m& one bays of length 5.5m along Y - direction are provided. Shear Wall is provided at the center core of building model.

3.2 Load Combinations

As per IS 1893 (Part 1): 2002 Clause no. 6.3.1.2, the following load cases have to be considered for analysis:

1.5 (DL + IL)

1.2 (DL + IL ± EL)

1.5 (DL ± EL)

0.9 DL ± 1.5 EL

Earthquake load must be considered for +X, -X, +Y and -Y directions.

Table 1 : Details of The Building

| Building Parameters | Details |
|---------------------------|---|
| Type of frame | Special RC moment resisting frame fixed at the base |
| Building plan | 38.5m X 35.5m |
| Number of storeys | 30 |
| Floor height | 3.5 m |
| Depth of Slab | 225 mm |
| Size of beam | (300 × 600) mm |
| Size of column (exterior) | (1250×1250) mm up to story five |
| Size of column (exterior) | (900×900) mm Above story five |
| Size of column (interior) | (1250×1250) mm up to story ten |
| Size of column (interior) | (900×900) mm Above story ten |
| Spacing between frames | 7.5-8.5 m along x - direction 7.5-5.5 m along y - direction |
| Live load on floor | 4 KN/m ² |
| Floor finish | 2.5 KN/m ² |
| Wall load | 25 KN/m |
| Grade of Concrete | M 50 concrete |
| Grade of Steel | Fe 500 |
| Thickness of shear wall | 450 mm |
| Seismic zone | V |
| Density of concrete | 25 KN/m ³ |
| Type of soil | Soft,Medium,Hard Soil Type I=Soft Soil Soil Type II=Medium Soil Soil Type III= Hard Soil |
| Response spectra | As per IS 1893(Part-1):2002 |
| Damping of structure | 5 percent |

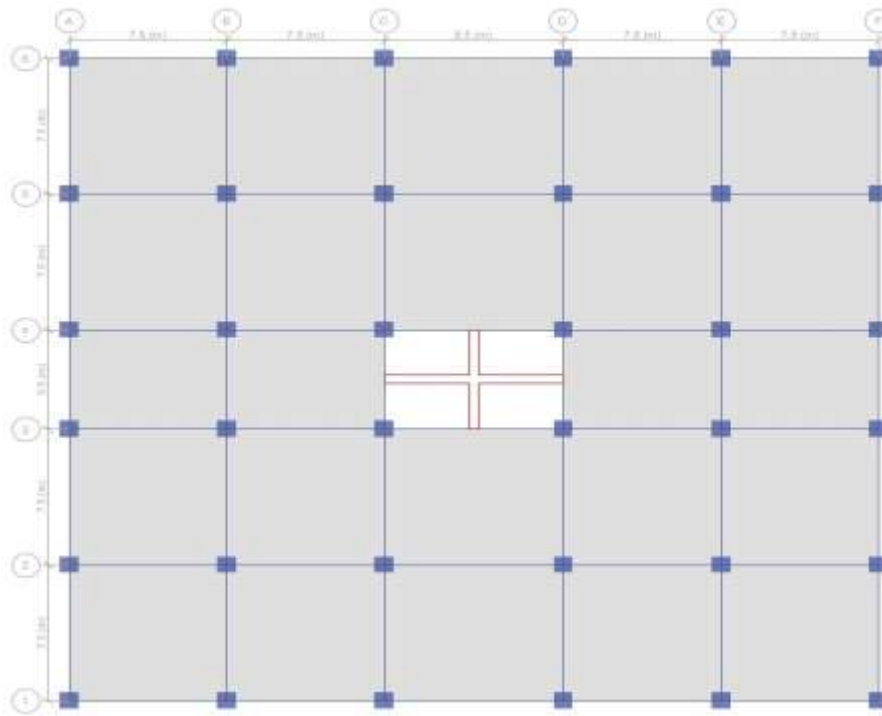


Figure 1. Plan of the building

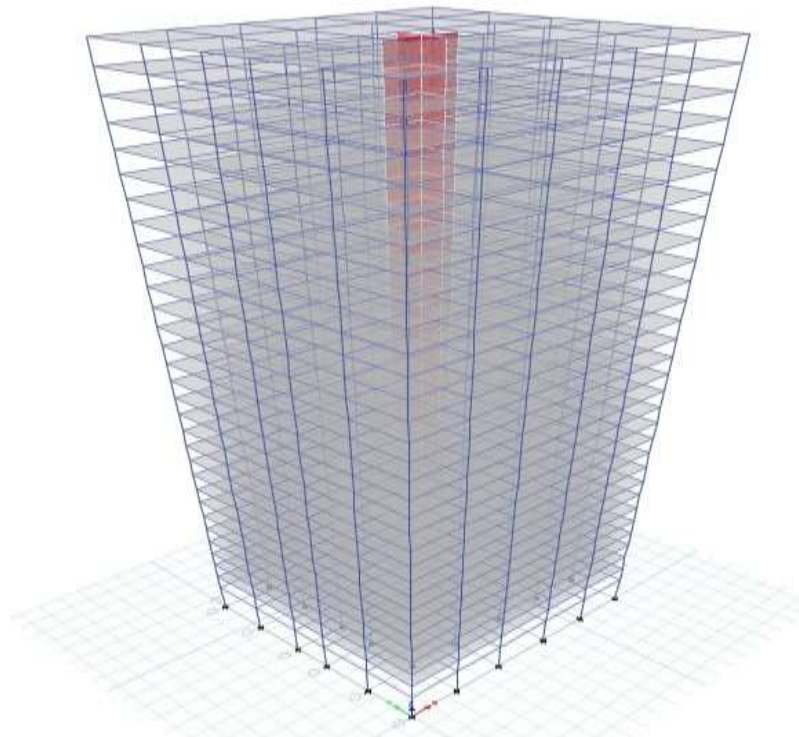


Figure 2. 3D view showing shear wall location

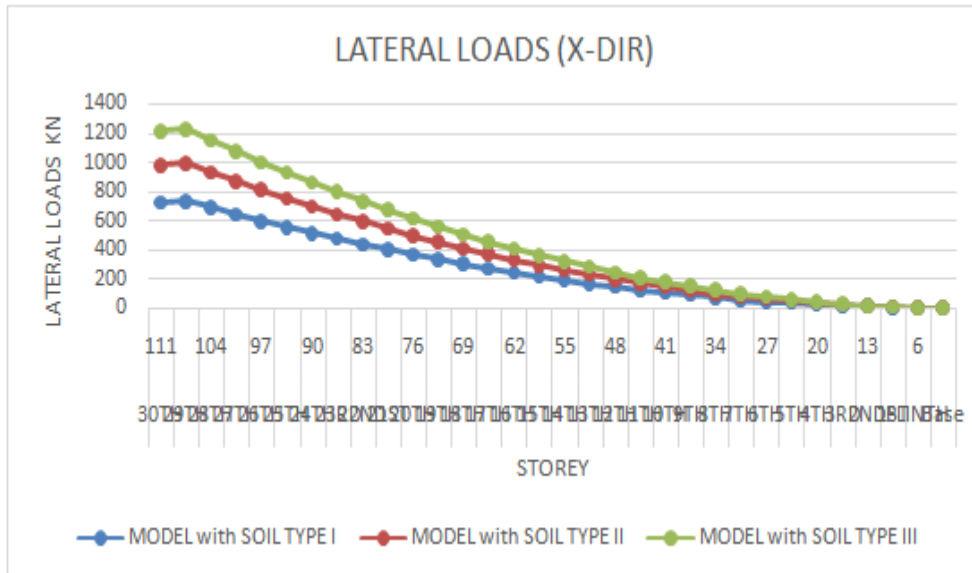
IV. RESULTS AND DISCUSSIONS

Table 2: Lateral Loads of Structure in Soft Soil , Medium Soil and Hard Soil in X –Direction for load cases EQXP

| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|----------------|----------|-------------|--------------|---------------|
| | | | X-Dir kN | X-Dir kN | X-Dir kN |
| 30TH | 111 | Top | 725.0746 | 986.1014 | 1210.8746 |
| 29TH | 107.5 | Top | 735.3706 | 1000.104 | 1228.0688 |
| 28TH | 104 | Top | 688.2655 | 936.0411 | 1149.4034 |

| | | | | | |
|--------|-------|-----|----------|----------|-----------|
| 27TH | 100.5 | Top | 642.7194 | 874.0984 | 1073.3415 |
| 26TH | 97 | Top | 598.7324 | 814.2761 | 999.8832 |
| 25TH | 93.5 | Top | 556.3045 | 756.5741 | 929.0284 |
| 24TH | 90 | Top | 515.4355 | 700.9923 | 860.7773 |
| 23RD | 86.5 | Top | 476.1256 | 647.5308 | 795.1297 |
| 22ND | 83 | Top | 438.3747 | 596.1896 | 732.0858 |
| 21ST | 79.5 | Top | 402.1829 | 546.9687 | 671.6454 |
| 20TH | 76 | Top | 367.5501 | 499.8681 | 613.8086 |
| 19TH | 72.5 | Top | 334.4763 | 454.8877 | 558.5754 |
| 18TH | 69 | Top | 302.9615 | 412.0277 | 505.9458 |
| 17TH | 65.5 | Top | 273.0058 | 371.2879 | 455.9197 |
| 16TH | 62 | Top | 244.6091 | 332.6684 | 408.4973 |
| 15TH | 58.5 | Top | 217.7715 | 296.1692 | 363.6784 |
| 14TH | 55 | Top | 192.4929 | 261.7903 | 321.4631 |
| 13TH | 51.5 | Top | 168.7733 | 229.5317 | 281.8514 |
| 12TH | 48 | Top | 146.6128 | 199.3934 | 244.8433 |
| 11TH | 44.5 | Top | 126.0113 | 171.3753 | 210.4388 |
| 10TH | 41 | Top | 108.2038 | 147.1571 | 180.7003 |
| 9TH | 37.5 | Top | 91.6609 | 124.6588 | 153.0737 |
| 8TH | 34 | Top | 75.3493 | 102.4751 | 125.8334 |
| 7TH | 30.5 | Top | 60.6347 | 82.4632 | 101.26 |
| 6TH | 27 | Top | 47.517 | 64.6231 | 79.3534 |
| 5TH | 23.5 | Top | 37.0427 | 50.3781 | 61.8614 |
| 4TH | 20 | Top | 27.6428 | 37.5942 | 46.1635 |
| 3RD | 16.5 | Top | 18.8144 | 25.5876 | 31.42 |
| 2ND | 13 | Top | 11.6791 | 15.8836 | 19.5041 |
| 1ST | 9.5 | Top | 6.2369 | 8.4822 | 10.4156 |
| PLINTH | 6 | Top | 1.3465 | 1.8312 | 2.2486 |
| Base | 0 | Top | 0 | 0 | 0 |

A plot for Lateral Loads of Structure in Soft Soil , Medium Soil and Hard Soil in X –Direction for load cases EQXP has been shown here



Graph 1: Lateral Loads of Structure in Soft Soil , Medium Soil and Hard Soil in X –Direction

Table 3: Stiffness of Structure in Soft Soil , Medium Soil and Hard Soil in X – Direction for load cases EQXP

| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|----------------|----------|---------------|---------------|---------------|
| | | | X-Dir kN/m | X-Dir kN/m | X-Dir kN/m |
| 30TH | 111 | Top | 143022.831 | 143022.831 | 143022.831 |
| 29TH | 107.5 | Top | 270359.127 | 270359.127 | 270359.127 |
| 28TH | 104 | Top | 381794.982 | 381794.982 | 381794.982 |
| 27TH | 100.5 | Top | 472732.209 | 472732.209 | 472732.209 |
| 26TH | 97 | Top | 545503.246 | 545503.246 | 545503.246 |
| 25TH | 93.5 | Top | 603792.812 | 603792.812 | 603792.812 |
| 24TH | 90 | Top | 650454.136 | 650454.136 | 650454.136 |
| 23RD | 86.5 | Top | 688057.119 | 688057.119 | 688057.119 |

| | | | | | |
|--------|------|-----|-------------|-------------|-------------|
| 22ND | 83 | Top | 718725.486 | 718725.486 | 718725.486 |
| 21ST | 79.5 | Top | 744162.046 | 744162.046 | 744162.046 |
| 20TH | 76 | Top | 765727.986 | 765727.986 | 765727.986 |
| 19TH | 72.5 | Top | 784518.418 | 784518.418 | 784518.418 |
| 18TH | 69 | Top | 801430.979 | 801430.979 | 801430.979 |
| 17TH | 65.5 | Top | 817225.311 | 817225.311 | 817225.311 |
| 16TH | 62 | Top | 832574.637 | 832574.637 | 832574.637 |
| 15TH | 58.5 | Top | 848111.52 | 848111.52 | 848111.52 |
| 14TH | 55 | Top | 864462.491 | 864462.491 | 864462.491 |
| 13TH | 51.5 | Top | 882365.473 | 882365.473 | 882365.473 |
| 12TH | 48 | Top | 902632.028 | 902632.028 | 902632.028 |
| 11TH | 44.5 | Top | 925075.51 | 925075.51 | 925075.51 |
| 10TH | 41 | Top | 956816.406 | 956816.406 | 956816.406 |
| 9TH | 37.5 | Top | 988643.743 | 988643.743 | 988643.743 |
| 8TH | 34 | Top | 1030418.09 | 1030418.09 | 1030418.09 |
| 7TH | 30.5 | Top | 1083371.397 | 1083371.397 | 1083371.397 |
| 6TH | 27 | Top | 1154692.733 | 1154692.733 | 1154692.733 |
| 5TH | 23.5 | Top | 1258596.787 | 1258596.787 | 1258596.787 |
| 4TH | 20 | Top | 1375721.385 | 1375721.385 | 1375721.385 |
| 3RD | 16.5 | Top | 1560244.267 | 1560244.267 | 1560244.267 |
| 2ND | 13 | Top | 1857338.108 | 1857338.108 | 1857338.108 |
| 1ST | 9.5 | Top | 2395459.119 | 2395459.119 | 2395459.119 |
| PLINTH | 6 | Top | 3052958.805 | 3052958.805 | 3052958.805 |
| Base | 0 | Top | 0 | 0 | 0 |

Table 4:Stiffness of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction for load cases EQYP

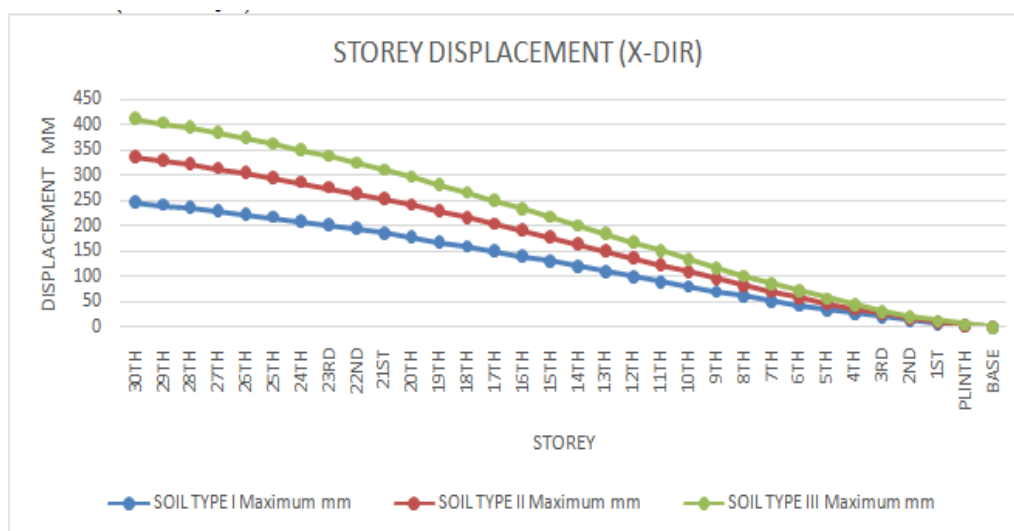
| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|--------|----------------|----------|---------------|---------------|---------------|
| | | | Y-Dir kN/m | Y-Dir kN/m | Y-Dir kN/m |
| 30TH | 111 | Top | 164522.123 | 164522.123 | 164522.123 |
| 29TH | 107.5 | Top | 302993.412 | 302993.412 | 302993.412 |
| 28TH | 104 | Top | 408677.202 | 408677.202 | 408677.202 |
| 27TH | 100.5 | Top | 483340.501 | 483340.501 | 483340.501 |
| 26TH | 97 | Top | 535680.552 | 535680.552 | 535680.552 |
| 25TH | 93.5 | Top | 572640.814 | 572640.814 | 572640.814 |
| 24TH | 90 | Top | 599109.141 | 599109.141 | 599109.141 |
| 23RD | 86.5 | Top | 618482.871 | 618482.871 | 618482.871 |
| 22ND | 83 | Top | 633043.22 | 633043.22 | 633043.22 |
| 21ST | 79.5 | Top | 644330.251 | 644330.251 | 644330.251 |
| 20TH | 76 | Top | 653399.721 | 653399.721 | 653399.721 |
| 19TH | 72.5 | Top | 660994.311 | 660994.311 | 660994.311 |
| 18TH | 69 | Top | 667657.281 | 667657.281 | 667657.281 |
| 17TH | 65.5 | Top | 673808.885 | 673808.885 | 673808.885 |
| 16TH | 62 | Top | 679800.36 | 679800.36 | 679800.36 |
| 15TH | 58.5 | Top | 685957.017 | 685957.017 | 685957.017 |
| 14TH | 55 | Top | 692607.423 | 692607.423 | 692607.423 |
| 13TH | 51.5 | Top | 700142.534 | 700142.534 | 700142.534 |
| 12TH | 48 | Top | 709147.826 | 709147.826 | 709147.826 |
| 11TH | 44.5 | Top | 719304.159 | 719304.159 | 719304.159 |
| 10TH | 41 | Top | 736444.19 | 736444.19 | 736444.19 |
| 9TH | 37.5 | Top | 752520.322 | 752520.322 | 752520.322 |
| 8TH | 34 | Top | 774346.165 | 774346.165 | 774346.165 |
| 7TH | 30.5 | Top | 803524.748 | 803524.748 | 803524.748 |
| 6TH | 27 | Top | 844489.543 | 844489.543 | 844489.543 |
| 5TH | 23.5 | Top | 906254.456 | 906254.456 | 906254.456 |
| 4TH | 20 | Top | 973343.501 | 973343.501 | 973343.501 |
| 3RD | 16.5 | Top | 1080765.084 | 1080765.084 | 1080765.084 |
| 2ND | 13 | Top | 1262128.804 | 1262128.804 | 1262128.804 |
| 1ST | 9.5 | Top | 1611231.402 | 1611231.402 | 1611231.402 |
| PLINTH | 6 | Top | 2029896.11 | 2029896.11 | 2029896.11 |
| Base | 0 | Top | 0 | 0 | 0 |

Table 5:StoreyDisplacement of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination (DL+LL+EQXP)

| | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|--|-------------|--------------|---------------|
|--|-------------|--------------|---------------|

| Story | Load Case/Combo | Direction | Story Maximum Displacements | Story Maximum Displacements | Story Maximum Displacements |
|--------|-----------------|-----------|-----------------------------|-----------------------------|-----------------------------|
| | | | mm | mm | mm |
| 30TH | DLLLEQXP | X | 247.583 | 336.596 | 413.247 |
| 29TH | DLLLEQXP | X | 242.298 | 329.414 | 404.43 |
| 28TH | DLLLEQXP | X | 236.611 | 321.685 | 394.942 |
| 27TH | DLLLEQXP | X | 230.622 | 313.544 | 384.95 |
| 26TH | DLLLEQXP | X | 224.275 | 304.917 | 374.358 |
| 25TH | DLLLEQXP | X | 217.536 | 295.757 | 363.114 |
| 24TH | DLLLEQXP | X | 210.398 | 286.054 | 351.202 |
| 23RD | DLLLEQXP | X | 202.862 | 275.81 | 338.626 |
| 22ND | DLLLEQXP | X | 194.94 | 265.041 | 325.405 |
| 21ST | DLLLEQXP | X | 186.65 | 253.771 | 311.57 |
| 20TH | DLLLEQXP | X | 178.016 | 242.034 | 297.161 |
| 19TH | DLLLEQXP | X | 169.068 | 229.869 | 282.226 |
| 18TH | DLLLEQXP | X | 159.836 | 217.319 | 266.818 |
| 17TH | DLLLEQXP | X | 150.356 | 204.431 | 250.996 |
| 16TH | DLLLEQXP | X | 140.667 | 191.258 | 234.823 |
| 15TH | DLLLEQXP | X | 130.807 | 177.854 | 218.366 |
| 14TH | DLLLEQXP | X | 120.821 | 164.277 | 201.697 |
| 13TH | DLLLEQXP | X | 110.754 | 150.59 | 184.893 |
| 12TH | DLLLEQXP | X | 100.656 | 136.861 | 168.037 |
| 11TH | DLLLEQXP | X | 90.581 | 123.163 | 151.219 |
| 10TH | DLLLEQXP | X | 80.58 | 109.565 | 134.524 |
| 9TH | DLLLEQXP | X | 70.768 | 96.224 | 118.145 |
| 8TH | DLLLEQXP | X | 61.148 | 83.144 | 102.085 |
| 7TH | DLLLEQXP | X | 51.811 | 70.449 | 86.498 |
| 6TH | DLLLEQXP | X | 42.845 | 58.259 | 71.531 |
| 5TH | DLLLEQXP | X | 34.377 | 46.744 | 57.393 |
| 4TH | DLLLEQXP | X | 26.571 | 36.13 | 44.362 |
| 3RD | DLLLEQXP | X | 19.376 | 26.348 | 32.351 |
| 2ND | DLLLEQXP | X | 12.981 | 17.651 | 21.673 |
| 1ST | DLLLEQXP | X | 7.564 | 10.286 | 12.63 |
| PLINTH | DLLLEQXP | X | 3.951 | 4.831 | 5.241 |
| BASE | DLLLEQXP | X | 0 | 0 | 0 |

A plot for Storey Displacement of Structure in Soft Soil, Medium Soil and Hard Soil in X - Direction with load combination (DL+LL+EQXP) has been shown here



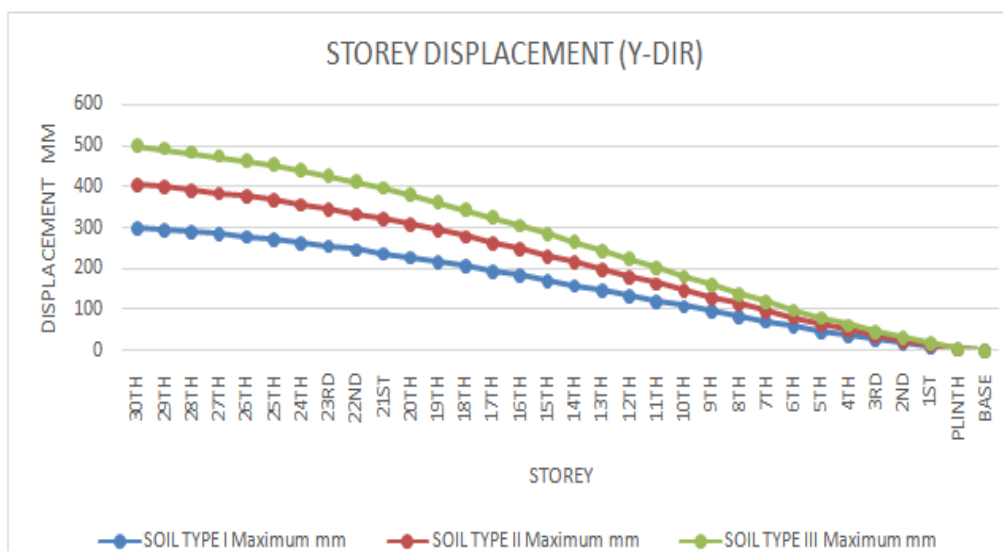
Graph 2: Storey Displacement of Structure in Soft Soil, Medium Soil and Hard Soil in X - Direction

Table 6: Storey Displacement of Structure in Soft Soil, Medium Soil and Hard Soil in Y - Direction with load combination (DL+LL+EQYP)

| Story | Load Case/Combo | Direction | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|-----------------|-----------|-----------------------------|-----------------------------|-----------------------------|
| | | | Story Maximum Displacements | Story Maximum Displacements | Story Maximum Displacements |
| | | | mm | mm | mm |

| | | | | | |
|--------|----------|---|---------|---------|---------|
| 30TH | DLLLEQYP | Y | 298.758 | 407.017 | 500.24 |
| 29TH | DLLLEQYP | Y | 294.166 | 400.75 | 492.53 |
| 28TH | DLLLEQYP | Y | 289.096 | 393.829 | 484.016 |
| 27TH | DLLLEQYP | Y | 283.5 | 386.194 | 474.624 |
| 26TH | DLLLEQYP | Y | 277.293 | 377.726 | 464.21 |
| 25TH | DLLLEQYP | Y | 270.439 | 368.377 | 452.712 |
| 24TH | DLLLEQYP | Y | 262.93 | 358.137 | 440.122 |
| 23RD | DLLLEQYP | Y | 254.778 | 347.024 | 426.459 |
| 22ND | DLLLEQYP | Y | 246.009 | 335.071 | 411.763 |
| 21ST | DLLLEQYP | Y | 236.656 | 322.324 | 396.093 |
| 20TH | DLLLEQYP | Y | 226.758 | 308.835 | 379.512 |
| 19TH | DLLLEQYP | Y | 216.358 | 294.664 | 362.094 |
| 18TH | DLLLEQYP | Y | 205.503 | 279.874 | 343.915 |
| 17TH | DLLLEQYP | Y | 194.239 | 264.527 | 325.054 |
| 16TH | DLLLEQYP | Y | 182.615 | 248.692 | 305.592 |
| 15TH | DLLLEQYP | Y | 170.681 | 232.436 | 285.613 |
| 14TH | DLLLEQYP | Y | 158.489 | 215.828 | 265.204 |
| 13TH | DLLLEQYP | Y | 146.092 | 198.943 | 244.453 |
| 12TH | DLLLEQYP | Y | 133.548 | 181.858 | 223.457 |
| 11TH | DLLLEQYP | Y | 120.921 | 164.66 | 202.324 |
| 10TH | DLLLEQYP | Y | 108.27 | 147.429 | 181.15 |
| 9TH | DLLLEQYP | Y | 95.744 | 130.371 | 160.188 |
| 8TH | DLLLEQYP | Y | 83.342 | 113.481 | 139.433 |
| 7TH | DLLLEQYP | Y | 71.167 | 96.901 | 119.061 |
| 6TH | DLLLEQYP | Y | 59.342 | 80.798 | 99.273 |
| 5TH | DLLLEQYP | Y | 48.031 | 65.395 | 80.347 |
| 4TH | DLLLEQYP | Y | 37.459 | 50.999 | 62.659 |
| 3RD | DLLLEQYP | Y | 27.565 | 37.527 | 46.106 |
| 2ND | DLLLEQYP | Y | 18.609 | 25.333 | 31.123 |
| 1ST | DLLLEQYP | Y | 10.901 | 14.839 | 18.23 |
| PLINTH | DLLLEQXP | Y | 2.443 | 3.614 | 4.39 |
| BASE | DLLLEQXP | Y | 0 | 0 | 0 |

A plot for StoreyDisplacement of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction with load combination (DL+LL+EQYP) has been shown here



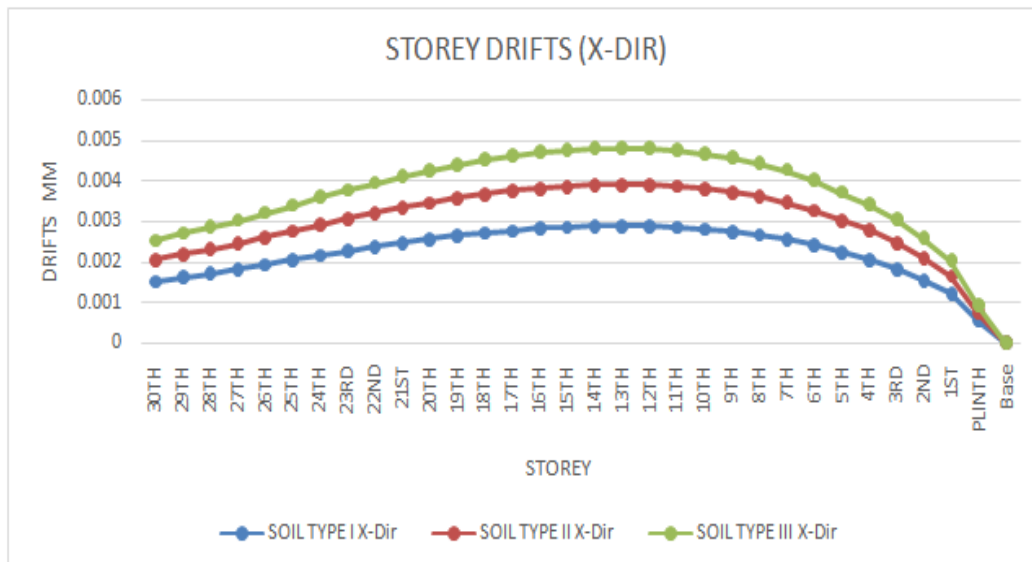
Graph 3: StoreyDisplacement of Structure in Soft Soil , Medium Soil and Hard Soil in Y – DirectionFor both X and Y directions, the behaviour of the graph is similar for model in Soft Soil , Medium Soil and Hard Soil as shown. The order of maximum storey displacement in both the directions for the models is same.

Table 7:StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination (DL+LL+EQXP)

| Story | Elevation | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|-----------|----------|-------------|--------------|---------------|
| | | | X-Dir | X-Dir | X-Dir |
| 30TH | 111 | Top | 0.001515 | 0.002059 | 0.002527 |
| 29TH | 107.5 | Top | 0.001625 | 0.002208 | 0.002711 |

| | | | | | |
|--------|-------|-----|----------|----------|----------|
| 28TH | 104 | Top | 0.001711 | 0.002326 | 0.002855 |
| 27TH | 100.5 | Top | 0.001814 | 0.002465 | 0.003026 |
| 26TH | 97 | Top | 0.001925 | 0.002617 | 0.003213 |
| 25TH | 93.5 | Top | 0.00204 | 0.002772 | 0.003403 |
| 24TH | 90 | Top | 0.002153 | 0.002927 | 0.003593 |
| 23RD | 86.5 | Top | 0.002263 | 0.003077 | 0.003777 |
| 22ND | 83 | Top | 0.002369 | 0.00322 | 0.003953 |
| 21ST | 79.5 | Top | 0.002467 | 0.003353 | 0.004117 |
| 20TH | 76 | Top | 0.002557 | 0.003476 | 0.004267 |
| 19TH | 72.5 | Top | 0.002638 | 0.003586 | 0.004402 |
| 18TH | 69 | Top | 0.002708 | 0.003682 | 0.004521 |
| 17TH | 65.5 | Top | 0.002768 | 0.003764 | 0.004621 |
| 16TH | 62 | Top | 0.002817 | 0.00383 | 0.004702 |
| 15TH | 58.5 | Top | 0.002853 | 0.003879 | 0.004762 |
| 14TH | 55 | Top | 0.002876 | 0.003911 | 0.004801 |
| 13TH | 51.5 | Top | 0.002885 | 0.003923 | 0.004816 |
| 12TH | 48 | Top | 0.002879 | 0.003914 | 0.004805 |
| 11TH | 44.5 | Top | 0.002858 | 0.003885 | 0.00477 |
| 10TH | 41 | Top | 0.002803 | 0.003812 | 0.00468 |
| 9TH | 37.5 | Top | 0.002749 | 0.003737 | 0.004588 |
| 8TH | 34 | Top | 0.002668 | 0.003627 | 0.004454 |
| 7TH | 30.5 | Top | 0.002562 | 0.003483 | 0.004276 |
| 6TH | 27 | Top | 0.00242 | 0.00329 | 0.004039 |
| 5TH | 23.5 | Top | 0.00223 | 0.003032 | 0.003723 |
| 4TH | 20 | Top | 0.002056 | 0.002795 | 0.003432 |
| 3RD | 16.5 | Top | 0.001827 | 0.002485 | 0.003051 |
| 2ND | 13 | Top | 0.001548 | 0.002104 | 0.002584 |
| 1ST | 9.5 | Top | 0.00122 | 0.001656 | 0.002031 |
| PLINTH | 6 | Top | 0.00056 | 0.00076 | 0.000932 |
| Base | 0 | Top | 0 | 0 | 0 |

A plot for StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination (DL+LL+EQXP) has been shown here



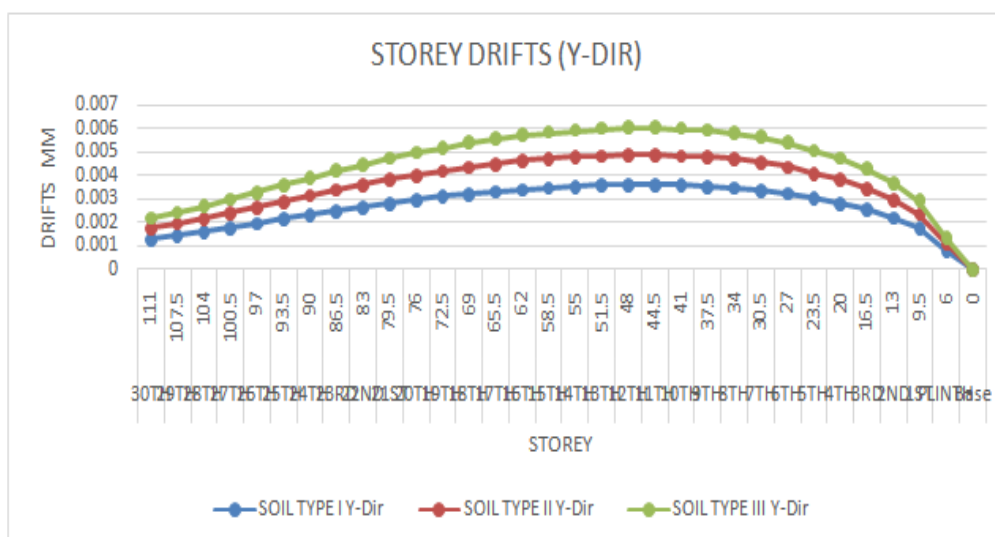
Graph 4: StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction

Table 8: StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction with load combination (DL+LL+EQYP)

| Story | Elevation | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|-----------|----------|-------------|--------------|---------------|
| | | | Y-Dir | Y-Dir | Y-Dir |
| 30TH | 111 | Top | 0.001312 | 0.001791 | 0.002203 |
| 29TH | 107.5 | Top | 0.001449 | 0.001977 | 0.002433 |
| 28TH | 104 | Top | 0.001599 | 0.002182 | 0.002683 |
| 27TH | 100.5 | Top | 0.001773 | 0.002419 | 0.002976 |
| 26TH | 97 | Top | 0.001958 | 0.002671 | 0.003285 |
| 25TH | 93.5 | Top | 0.002145 | 0.002926 | 0.003597 |
| 24TH | 90 | Top | 0.002329 | 0.003175 | 0.003904 |
| 23RD | 86.5 | Top | 0.002505 | 0.003415 | 0.004199 |

| | | | | | |
|--------|------|-----|----------|----------|----------|
| 22ND | 83 | Top | 0.002672 | 0.003642 | 0.004477 |
| 21ST | 79.5 | Top | 0.002828 | 0.003854 | 0.004737 |
| 20TH | 76 | Top | 0.002971 | 0.004049 | 0.004977 |
| 19TH | 72.5 | Top | 0.003102 | 0.004226 | 0.005194 |
| 18TH | 69 | Top | 0.003218 | 0.004385 | 0.005389 |
| 17TH | 65.5 | Top | 0.003321 | 0.004524 | 0.005561 |
| 16TH | 62 | Top | 0.00341 | 0.004645 | 0.005708 |
| 15TH | 58.5 | Top | 0.003483 | 0.004745 | 0.005831 |
| 14TH | 55 | Top | 0.003542 | 0.004824 | 0.005929 |
| 13TH | 51.5 | Top | 0.003584 | 0.004882 | 0.005999 |
| 12TH | 48 | Top | 0.003608 | 0.004914 | 0.006038 |
| 11TH | 44.5 | Top | 0.003615 | 0.004923 | 0.00605 |
| 10TH | 41 | Top | 0.003579 | 0.004874 | 0.005989 |
| 9TH | 37.5 | Top | 0.003544 | 0.004826 | 0.00593 |
| 8TH | 34 | Top | 0.003478 | 0.004737 | 0.005821 |
| 7TH | 30.5 | Top | 0.003379 | 0.004601 | 0.005654 |
| 6TH | 27 | Top | 0.003232 | 0.004401 | 0.005407 |
| 5TH | 23.5 | Top | 0.003021 | 0.004113 | 0.005054 |
| 4TH | 20 | Top | 0.002827 | 0.003849 | 0.004729 |
| 3RD | 16.5 | Top | 0.002559 | 0.003484 | 0.004281 |
| 2ND | 13 | Top | 0.002202 | 0.002998 | 0.003684 |
| 1ST | 9.5 | Top | 0.001748 | 0.002376 | 0.002917 |
| PLINTH | 6 | Top | 0.00081 | 0.001102 | 0.001354 |
| Base | 0 | Top | 0 | 0 | 0 |

A plot for StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction with load combination (DL+LL+EQYP) has been shown here



Graph 5: StoreyDrifts of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction

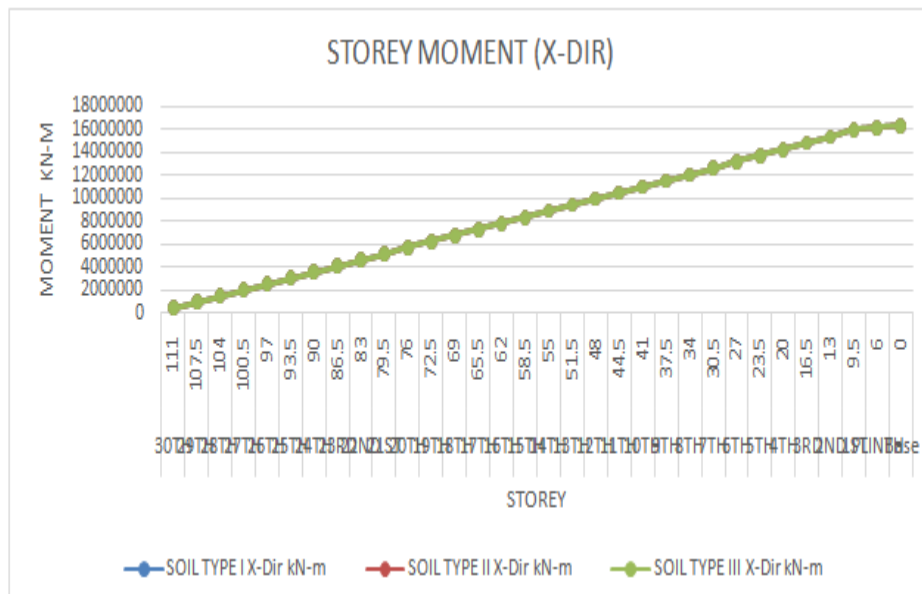
As per Indian standard, Criteria for earthquake resistant design of structures, IS 1893 (Part 1) : 2002, the story drift in any story due to service load shall not exceed 0.004 times the story height. The height of the each storey is 3.5 m. So, the drift limitation as per IS 1893 (part 1) : 2002 is 0.004 X 3.5 m = 14 mm. The model show a similar behaviour for storey drifts as shown in graph.

Table 9: Storey Moment of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination 1.2(DL+LL+EQXP)

| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|----------------|----------|---------------|---------------|---------------|
| | | | X-Dir kN-m | X-Dir kN-m | X-Dir kN-m |
| 30TH | 111 | Top | 465614.6719 | 465614.6719 | 465614.6719 |
| 29TH | 107.5 | Top | 995789.2594 | 995789.2594 | 995789.2594 |
| 28TH | 104 | Top | 1525964 | 1525964 | 1525964 |
| 27TH | 100.5 | Top | 2056138 | 2056138 | 2056138 |
| 26TH | 97 | Top | 2586313 | 2586313 | 2586313 |
| 25TH | 93.5 | Top | 3116488 | 3116488 | 3116488 |
| 24TH | 90 | Top | 3646662 | 3646662 | 3646662 |

| | | | | | |
|--------|------|-----|----------|----------|----------|
| 23RD | 86.5 | Top | 4176837 | 4176837 | 4176837 |
| 22ND | 83 | Top | 4707011 | 4707011 | 4707011 |
| 21ST | 79.5 | Top | 5237186 | 5237186 | 5237186 |
| 20TH | 76 | Top | 5767361 | 5767361 | 5767361 |
| 19TH | 72.5 | Top | 6297535 | 6297535 | 6297535 |
| 18TH | 69 | Top | 6827710 | 6827710 | 6827710 |
| 17TH | 65.5 | Top | 7357884 | 7357884 | 7357884 |
| 16TH | 62 | Top | 7888059 | 7888059 | 7888059 |
| 15TH | 58.5 | Top | 8418233 | 8418233 | 8418233 |
| 14TH | 55 | Top | 8948408 | 8948408 | 8948408 |
| 13TH | 51.5 | Top | 9478583 | 9478583 | 9478583 |
| 12TH | 48 | Top | 10008757 | 10008757 | 10008757 |
| 11TH | 44.5 | Top | 10538932 | 10538932 | 10538932 |
| 10TH | 41 | Top | 11068570 | 11068570 | 11068570 |
| 9TH | 37.5 | Top | 11609427 | 11609427 | 11609427 |
| 8TH | 34 | Top | 12150285 | 12150285 | 12150285 |
| 7TH | 30.5 | Top | 12691142 | 12691142 | 12691142 |
| 6TH | 27 | Top | 13232000 | 13232000 | 13232000 |
| 5TH | 23.5 | Top | 13771918 | 13771918 | 13771918 |
| 4TH | 20 | Top | 14339886 | 14339886 | 14339886 |
| 3RD | 16.5 | Top | 14907854 | 14907854 | 14907854 |
| 2ND | 13 | Top | 15475821 | 15475821 | 15475821 |
| 1ST | 9.5 | Top | 16043789 | 16043789 | 16043789 |
| PLINTH | 6 | Top | 16264437 | 16264437 | 16264437 |
| Base | 0 | Top | 16445051 | 16445051 | 16445051 |

A plot for Storey Moment of Structure in Soft Soil, Medium Soil and Hard Soil in X - Direction with load combination 1.2(DL+LL+EXP) has been shown here



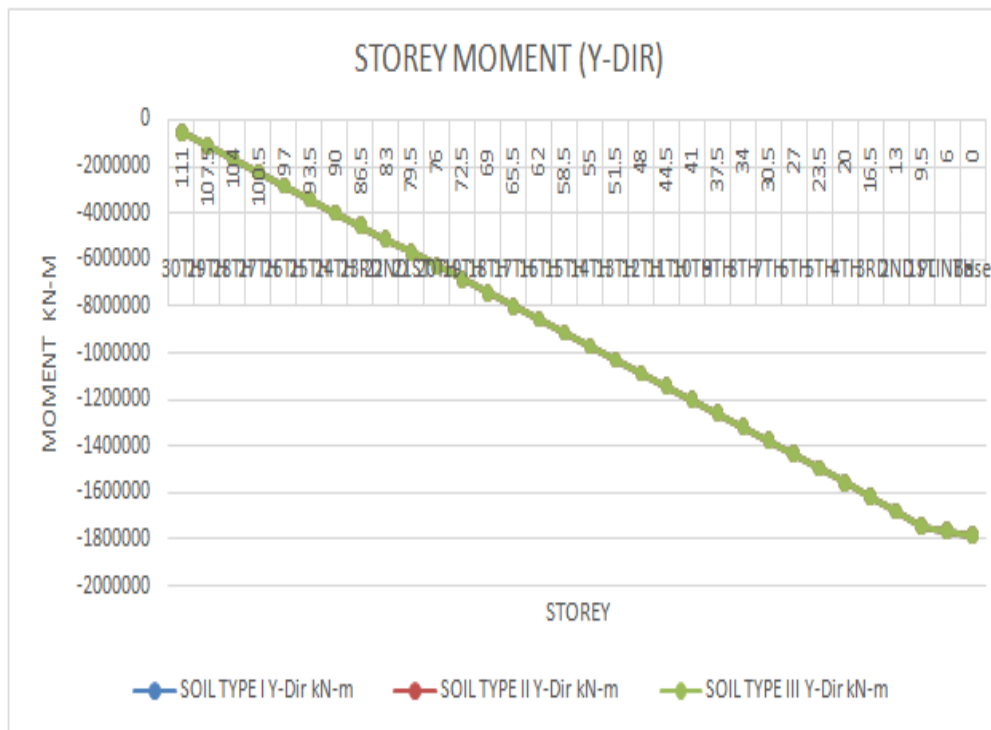
Graph 6: Storey Moment of Structure in Soft Soil, Medium Soil and Hard Soil in X - Direction

Table 10: Storey Moment of Structure in Soft Soil, Medium Soil and Hard Soil in Y - Direction with load combination 1.2(DL+LL+EQYP)

| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|----------------|----------|---------------|---------------|---------------|
| | | | Y-Dir kN-m | Y-Dir kN-m | Y-Dir kN-m |
| 30TH | 111 | Top | -504851 | -504851 | -504851 |
| 29TH | 107.5 | Top | -1080107 | -1080107 | -1080107 |
| 28TH | 104 | Top | -1655363 | -1655363 | -1655363 |
| 27TH | 100.5 | Top | -2230620 | -2230620 | -2230620 |
| 26TH | 97 | Top | -2805876 | -2805876 | -2805876 |
| 25TH | 93.5 | Top | -3381133 | -3381133 | -3381133 |
| 24TH | 90 | Top | -3956389 | -3956389 | -3956389 |
| 23RD | 86.5 | Top | -4531645 | -4531645 | -4531645 |

| | | | | | |
|--------|------|-----|-----------|-----------|-----------|
| 22ND | 83 | Top | -5106902 | -5106902 | -5106902 |
| 21ST | 79.5 | Top | -5682158 | -5682158 | -5682158 |
| 20TH | 76 | Top | -6257414 | -6257414 | -6257414 |
| 19TH | 72.5 | Top | -6832671 | -6832671 | -6832671 |
| 18TH | 69 | Top | -7407927 | -7407927 | -7407927 |
| 17TH | 65.5 | Top | -7983184 | -7983184 | -7983184 |
| 16TH | 62 | Top | -8558440 | -8558440 | -8558440 |
| 15TH | 58.5 | Top | -9133696 | -9133696 | -9133696 |
| 14TH | 55 | Top | -9708953 | -9708953 | -9708953 |
| 13TH | 51.5 | Top | -10284209 | -10284209 | -10284209 |
| 12TH | 48 | Top | -10859466 | -10859466 | -10859466 |
| 11TH | 44.5 | Top | -11434722 | -11434722 | -11434722 |
| 10TH | 41 | Top | -12009396 | -12009396 | -12009396 |
| 9TH | 37.5 | Top | -12596238 | -12596238 | -12596238 |
| 8TH | 34 | Top | -13183081 | -13183081 | -13183081 |
| 7TH | 30.5 | Top | -13769923 | -13769923 | -13769923 |
| 6TH | 27 | Top | -14356765 | -14356765 | -14356765 |
| 5TH | 23.5 | Top | -14942589 | -14942589 | -14942589 |
| 4TH | 20 | Top | -15558832 | -15558832 | -15558832 |
| 3RD | 16.5 | Top | -16175075 | -16175075 | -16175075 |
| 2ND | 13 | Top | -16791318 | -16791318 | -16791318 |
| 1ST | 9.5 | Top | -17407562 | -17407562 | -17407562 |
| PLINTH | 6 | Top | -17646856 | -17646856 | -17646856 |
| Base | 0 | Top | -17842733 | -17842733 | -17842733 |

A plot for Storey Moment of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction with load combination 1.2(DL+LL+EYP)has been shown here



Graph 7: Storey Moment of Structure in Soft Soil , Medium Soil and Hard Soil in Y - Direction

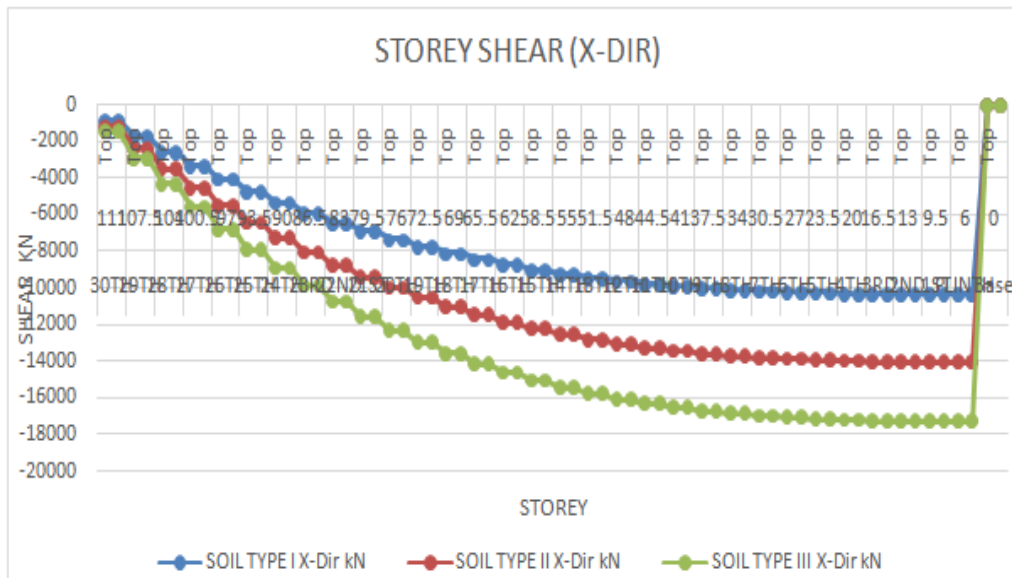
Table 11: Storey Shear of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination 1.2 (DL+LL+EQXP)

| Story | Elevation m | Location | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|-------|----------------|----------|-------------|--------------|---------------|
| | | | X-Dir kN | X-Dir kN | X-Dir kN |
| 30TH | 111 | Top | -870.0895 | -1183.3217 | -1453.0495 |
| | | Bottom | -870.0895 | -1183.3217 | -1453.0495 |
| 29TH | 107.5 | Top | -1752.5342 | -2383.4465 | -2926.7321 |
| | | Bottom | -1752.5342 | -2383.4465 | -2926.7321 |

| | | | | | |
|------|-------|--------|-------------|-------------|-------------|
| 28TH | 104 | Top | -2578.4528 | -3506.6958 | -4306.0161 |
| | | Bottom | -2578.4528 | -3506.6958 | -4306.0161 |
| 27TH | 100.5 | Top | -3349.7161 | -4555.6139 | -5594.0259 |
| | | Bottom | -3349.7161 | -4555.6139 | -5594.0259 |
| 26TH | 97 | Top | -4068.195 | -5532.7452 | -6793.8857 |
| | | Bottom | -4068.195 | -5532.7452 | -6793.8857 |
| 25TH | 93.5 | Top | -4735.7604 | -6440.6341 | -7908.7198 |
| | | Bottom | -4735.7604 | -6440.6341 | -7908.7198 |
| 24TH | 90 | Top | -5354.283 | -7281.8248 | -8941.6526 |
| | | Bottom | -5354.283 | -7281.8248 | -8941.6526 |
| 23RD | 86.5 | Top | -5925.6337 | -8058.8618 | -9895.8083 |
| | | Bottom | -5925.6337 | -8058.8618 | -9895.8083 |
| 22ND | 83 | Top | -6451.6833 | -8774.2894 | -10774.3112 |
| | | Bottom | -6451.6833 | -8774.2894 | -10774.3112 |
| 21ST | 79.5 | Top | -6934.3028 | -9430.6518 | -11580.2857 |
| | | Bottom | -6934.3028 | -9430.6518 | -11580.2857 |
| 20TH | 76 | Top | -7375.3629 | -10030.4935 | -12316.856 |
| | | Bottom | -7375.3629 | -10030.4935 | -12316.856 |
| 19TH | 72.5 | Top | -7776.7344 | -10576.3588 | -12987.1465 |
| | | Bottom | -7776.7344 | -10576.3588 | -12987.1465 |
| 18TH | 69 | Top | -8140.2883 | -11070.792 | -13594.2814 |
| | | Bottom | -8140.2883 | -11070.792 | -13594.2814 |
| 17TH | 65.5 | Top | -8467.8952 | -11516.3375 | -14141.3851 |
| | | Bottom | -8467.8952 | -11516.3375 | -14141.3851 |
| 16TH | 62 | Top | -8761.4262 | -11915.5397 | -14631.5818 |
| | | Bottom | -8761.4262 | -11915.5397 | -14631.5818 |
| 15TH | 58.5 | Top | -9022.752 | -12270.9427 | -15067.9959 |
| | | Bottom | -9022.752 | -12270.9427 | -15067.9959 |
| 14TH | 55 | Top | -9253.7435 | -12585.0911 | -15453.7516 |
| | | Bottom | -9253.7435 | -12585.0911 | -15453.7516 |
| 13TH | 51.5 | Top | -9456.2715 | -12860.5292 | -15791.9733 |
| | | Bottom | -9456.2715 | -12860.5292 | -15791.9733 |
| 12TH | 48 | Top | -9632.2068 | -13099.8012 | -16085.7853 |
| | | Bottom | -9632.2068 | -13099.8012 | -16085.7853 |
| 11TH | 44.5 | Top | -9783.4203 | -13305.4516 | -16338.3119 |
| | | Bottom | -9783.4203 | -13305.4516 | -16338.3119 |
| 10TH | 41 | Top | -9913.2648 | -13482.0401 | -16555.1522 |
| | | Bottom | -9913.2648 | -13482.0401 | -16555.1522 |
| 9TH | 37.5 | Top | -10023.2579 | -13631.6307 | -16738.8406 |
| | | Bottom | -10023.2579 | -13631.6307 | -16738.8406 |
| 8TH | 34 | Top | -10113.6771 | -13754.6008 | -16889.8407 |
| | | Bottom | -10113.6771 | -13754.6008 | -16889.8407 |
| 7TH | 30.5 | Top | -10186.4387 | -13853.5566 | -17011.3526 |
| | | Bottom | -10186.4387 | -13853.5566 | -17011.3526 |
| 6TH | 27 | Top | -10243.4591 | -13931.1044 | -17106.5767 |

| | | | | | |
|--------|------|--------|-------------|-------------|-------------|
| | | Bottom | -10243.4591 | -13931.1044 | -17106.5767 |
| 5TH | 23.5 | Top | -10287.9104 | -13991.5582 | -17180.8104 |
| | | Bottom | -10287.9104 | -13991.5582 | -17180.8104 |
| 4TH | 20 | Top | -10321.0818 | -14036.6713 | -17236.2066 |
| | | Bottom | -10321.0818 | -14036.6713 | -17236.2066 |
| 3RD | 16.5 | Top | -10343.6591 | -14067.3763 | -17273.9107 |
| | | Bottom | -10343.6591 | -14067.3763 | -17273.9107 |
| 2ND | 13 | Top | -10357.674 | -14086.4366 | -17297.3156 |
| | | Bottom | -10357.674 | -14086.4366 | -17297.3156 |
| 1ST | 9.5 | Top | -10365.1583 | -14096.6153 | -17309.8143 |
| | | Bottom | -10365.1583 | -14096.6153 | -17309.8143 |
| PLINTH | 6 | Top | -10366.7741 | -14098.8127 | -17312.5127 |
| | | Bottom | -10366.7741 | -14098.8127 | -17312.5127 |
| Base | 0 | Top | 0 | 0 | 0 |
| | | Bottom | 0 | 0 | 0 |

A plot for Storey Shear of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction with load combination 1.2(DL+LL+EXP) has been shown here



Graph 8: Storey Shear of Structure in Soft Soil , Medium Soil and Hard Soil in X - Direction

Column Forces

Table 12: column axial force, P for structure with the load combination 1.2 (DL+LL+EQXP) & 1.2 (DL+LL+EQYP) in soft ,medium &hard soil

| TABLE: Column Forces | | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|----------------------|--------|-------------|-----------------|--------------|-------------|--------------|---------------|
| Story | Column | Unique Name | Load Case/Combo | Station m | P kN | P kN | P kN |
| 1ST | C34 | 67 | 12DLRLLEQXP | 0 | -24171.1 | -24937.5 | -25597.5 |
| 1ST | C34 | 67 | 12DLRLLEQXP | 1.45 | -24103.1 | -24869.5 | -25529.5 |
| 1ST | C34 | 67 | 12DLRLLEQXP | 2.9 | -24035.1 | -24801.6 | -25461.5 |
| 1ST | C34 | 67 | 12DLRLLEQYP | 0 | -23630.6 | -24202.5 | -24695 |
| 1ST | C34 | 67 | 12DLRLLEQYP | 1.45 | -23562.7 | -24134.6 | -24627 |
| 1ST | C34 | 67 | 12DLRLLEQYP | 2.9 | -23494.7 | -24066.6 | -24559 |

Table 13:column Moment, M for structure with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft ,medium&hard soil

| TABLE: Column Forces | | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|----------------------|--------|-------------|-----------------|---------|-------------|--------------|---------------|-------------|--------------|---------------|
| Story | Column | Unique Name | Load Case/Combo | Station | M2 | M3 | M2 | M3 | M2 | M3 |
| | | | | m | kN-m | kN-m | kN-m | kN-m | kN-m | kN-m |
| 1ST | C34 | 67 | 12DLRLLQXP | 0 | -244.012 | 979.4715 | -312.524 | 1329.527 | -371.521 | 1630.963 |
| 1ST | C34 | 67 | 12DLRLLQXP | 1.45 | -146.268 | 805.6993 | -197.671 | 1112.772 | -241.934 | 1377.196 |
| 1ST | C34 | 67 | 12DLRLLQXP | 2.9 | -48.5251 | 631.9271 | -82.8175 | 896.0172 | -112.347 | 1123.428 |
| 1ST | C34 | 67 | 12DLRLLQYP | 0 | 1727.573 | -24.7075 | 2368.832 | -36.1568 | 2921.026 | -46.0159 |
| 1ST | C34 | 67 | 12DLRLLQYP | 1.45 | 1393.642 | -70.5194 | 1896.607 | -78.8855 | 2329.716 | -86.0897 |
| 1ST | C34 | 67 | 12DLRLLQYP | 2.9 | 1059.71 | -116.331 | 1424.382 | -121.614 | 1738.406 | -126.163 |

Table 14:column Shear , V for structure with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft ,medium &hard soil

| TABLE: Column Forces | | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|----------------------|--------|-------------|-----------------|---------|-------------|--------------|---------------|-------------|--------------|---------------|
| Story | Column | Unique Name | Load Case/Combo | Station | V2 | V3 | V2 | V3 | V2 | V3 |
| | | | | m | kN | kN | kN | kN | kN | kN |
| 1ST | C34 | 67 | 12DLRLLQXP | 0 | 119.8429 | -67.4092 | 149.486 | -79.2092 | 175.012 | -89.3703 |
| 1ST | C34 | 67 | 12DLRLLQXP | 1.45 | 119.8429 | -67.4092 | 149.486 | -79.2092 | 175.012 | -89.3703 |
| 1ST | C34 | 67 | 12DLRLLQXP | 2.9 | 119.8429 | -67.4092 | 149.486 | -79.2092 | 175.012 | -89.3703 |
| 1ST | C34 | 67 | 12DLRLLQYP | 0 | 31.5944 | 230.2977 | 29.4681 | 325.6722 | 27.6371 | 407.8002 |
| 1ST | C34 | 67 | 12DLRLLQYP | 1.45 | 31.5944 | 230.2977 | 29.4681 | 325.6722 | 27.6371 | 407.8002 |
| 1ST | C34 | 67 | 12DLRLLQYP | 2.9 | 31.5944 | 230.2977 | 29.4681 | 325.6722 | 27.6371 | 407.8002 |

Table 15:column Torsion , T for structure with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft ,medium &hard soil

| TABLE: Column Forces | | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|----------------------|--------|-------------|-----------------|---------|-------------|--------------|---------------|
| Story | Column | Unique Name | Load Case/Combo | Station | T | T | T |
| | | | | m | kN-m | kN-m | kN-m |
| 1ST | C34 | 67 | 12DLRLLQXP | 0 | -41.6175 | -56.5981 | -69.4981 |
| 1ST | C34 | 67 | 12DLRLLQXP | 1.45 | -41.6175 | -56.5981 | -69.4981 |
| 1ST | C34 | 67 | 12DLRLLQXP | 2.9 | -41.6175 | -56.5981 | -69.4981 |
| 1ST | C34 | 67 | 12DLRLLQYP | 0 | 45.3145 | 61.6294 | 75.6784 |
| 1ST | C34 | 67 | 12DLRLLQYP | 1.45 | 45.3145 | 61.6294 | 75.6784 |
| 1ST | C34 | 67 | 12DLRLLQYP | 2.9 | 45.3145 | 61.6294 | 75.6784 |

Pier Forces

Table 16: Pier Axial Force, P for structure with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft ,medium&hard soil

| TABLE: Pier Forces | | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|--------------------|------|-----------------|----------|-------------|-------------|--------------|---------------|
| Story | Pier | Load Case/Combo | Location | P | P | P | |
| | | | | kN | kN | kN | |
| 1ST | P3 | 12DLRLLQXP | Top | -31716.3887 | -31716.3887 | -31716.3887 | |
| 1ST | P3 | 12DLRLLQXP | Bottom | -31976.2637 | -31976.2637 | -31976.2637 | |
| 1ST | P3 | 12DLRLLQYP | Top | -31716.3887 | -31716.3887 | -31716.3887 | |
| 1ST | P3 | 12DLRLLQYP | Bottom | -31976.2637 | -31976.2637 | -31976.2637 | |

Table 17: Pier Moment, M for structure with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft ,medium &hard soil

| TABLE: Pier Forces | | | | | SOIL TYPE I | SOIL TYPE I | SOIL TYPE II | SOIL TYPE II | SOIL TYPE III | SOIL TYPE III |
|--------------------|------|-----------------|----------|-----------|-------------|-------------|--------------|--------------|---------------|---------------|
| Story | Pier | Load Case/Combo | Location | M2 | M3 | M2 | M3 | M2 | M3 | |
| | | | | kN-m | kN-m | kN-m | kN-m | kN-m | kN-m | |
| 1ST | P3 | 12DLRLLQXP | Top | 429.3134 | -285.376 | 587.5838 | -285.376 | 723.8721 | -285.376 | |
| 1ST | P3 | 12DLRLLQXP | Bottom | -796.6308 | -244.1397 | -1084.8797 | -244.1397 | 1333.0941 | -244.1397 | |
| 1ST | P3 | 12DLRLLQYP | Top | -10.3264 | 29494.5797 | -10.3264 | 40215.3638 | -10.3264 | 49447.15 | |
| 1ST | P3 | 12DLRLLQYP | Bottom | 4.0607 | 41193.3422 | 4.0607 | 56110.8357 | 4.0607 | 68956.455 | |

Table 18: Pier Shear Force, V for structure with the load combination 1.2 (DL+LL+EQXP) & 1.2 (DL+LL+EQYP) in soft ,medium&hard soil

| TABLE: Pier Forces | | | | SOIL TYPE I | SOIL TYPE I | SOIL TYPE II | SOIL TYPE II | SOIL TYPE III | SOIL TYPE III |
|--------------------|------|-----------------|----------|-------------|-------------|--------------|--------------|---------------|---------------|
| Story | Pier | Load Case/Combo | Location | V2 | V3 | V2 | V3 | V2 | V3 |
| | | | | kN | kN | kN | kN | kN | kN |
| 1ST | P3 | 12DLRLEQXP | Top | 11.7818 | -350.2698 | 11.7818 | -477.8467 | 11.7818 | -587.7046 |
| 1ST | P3 | 12DLRLEQXP | Bottom | 11.7818 | -350.2698 | 11.7818 | -477.8467 | 11.7818 | -587.7046 |
| 1ST | P3 | 12DLRLEQYP | Top | 3342.5036 | 4.1106 | 4541.5634 | 4.1106 | 5574.0871 | 4.1106 |
| 1ST | P3 | 12DLRLEQYP | Bottom | 3342.5036 | 4.1106 | 4541.5634 | 4.1106 | 5574.0871 | 4.1106 |

Table 19: Pier Torsion, T for structure with the load combination 1.2 (DL+LL+EQXP) & 1.2 (DL+LL+EQYP) in soft ,medium&hard soil

| TABLE: Pier Forces | | | | SOIL TYPE I | SOIL TYPE II | SOIL TYPE III |
|--------------------|------|-----------------|----------|-------------|--------------|---------------|
| Story | Pier | Load Case/Combo | Location | T | T | T |
| | | | | kN-m | kN-m | kN-m |
| 1ST | P3 | 12DLRLEQXP | Top | -57.8883 | -75.9256 | -91.4578 |
| 1ST | P3 | 12DLRLEQXP | Bottom | -57.8883 | -75.9256 | -91.4578 |
| 1ST | P3 | 12DLRLEQYP | Top | 46.5531 | 66.1147 | 82.9594 |
| 1ST | P3 | 12DLRLEQYP | Bottom | 46.5531 | 66.1147 | 82.9594 |

Table 20: Modal Load Participation Ratios

| TABLE: Modal Load Participation Ratios | | | | |
|--|--------------|------|--------|---------|
| Case | Item Type | Item | Static | Dynamic |
| | | | % | % |
| Modal | Acceleration | UX | 99.82 | 86.71 |
| Modal | Acceleration | UY | 99.79 | 87.46 |
| Modal | Acceleration | UZ | 0 | 0 |

According to IS-1893:2002 the number of modes to be used in the analysis should be such that the total sum of modal masses of all modes considered is at least 90 percent of the total seismic mass. Here the minimum modal mass is 86.71 percent.

Table 21: Modal Participating Mass Ratios

| Case | Mode | Period sec | UX | UY | UZ | RX | RY | RZ |
|-------|------|------------|--------|--------|----|--------|--------|--------|
| Modal | 1 | 6.298 | 0 | 0.7575 | 0 | 0.2499 | 0 | 0 |
| Modal | 2 | 6.248 | 0 | 0 | 0 | 0 | 0 | 0.7702 |
| Modal | 3 | 5.545 | 0.7329 | 0 | 0 | 0 | 0.2768 | 0 |
| Modal | 4 | 2.062 | 0 | 0 | 0 | 0 | 0 | 0.1046 |
| Modal | 5 | 1.952 | 0 | 0.1171 | 0 | 0.4414 | 0 | 0 |
| Modal | 6 | 1.603 | 0.1343 | 0 | 0 | 0 | 0.3985 | 0 |
| Modal | 7 | 1.191 | 0 | 0 | 0 | 0 | 0 | 0.0422 |
| Modal | 8 | 1.027 | 0 | 0.046 | 0 | 0.0794 | 0 | 0 |
| Modal | 9 | 0.803 | 0 | 0 | 0 | 0 | 0 | 0.0227 |
| Modal | 10 | 0.782 | 0.0528 | 0 | 0 | 0 | 0.0991 | 0 |
| Modal | 11 | 0.645 | 0 | 0.0255 | 0 | 0.0769 | 0 | 0 |
| Modal | 12 | 0.581 | 0 | 0 | 0 | 0 | 0 | 0.0141 |

Here the minimum modal mass for accelerations Ux and Uy is 86.71% and 87.46% respectively.

Table 22: Modal Periods and Frequencies

| TABLE: Modal Periods and Frequencies SOIL TYPE I | | | | SOIL TYPE II | SOIL TYPE II | SOIL TYPE III | SOIL TYPE III |
|--|------|--------|-----------|--------------|--------------|---------------|---------------|
| Case | Mode | Period | Frequency | Period | Frequency | Period | Frequency |
| | | sec | cyc/sec | sec | cyc/sec | sec | cyc/sec |
| Modal | 1 | 6.298 | 0.159 | 6.298 | 0.159 | 6.298 | 0.159 |
| Modal | 2 | 6.248 | 0.16 | 6.248 | 0.16 | 6.248 | 0.16 |
| Modal | 3 | 5.545 | 0.18 | 5.545 | 0.18 | 5.545 | 0.18 |
| Modal | 4 | 2.062 | 0.485 | 2.062 | 0.485 | 2.062 | 0.485 |
| Modal | 5 | 1.952 | 0.512 | 1.952 | 0.512 | 1.952 | 0.512 |
| Modal | 6 | 1.603 | 0.624 | 1.603 | 0.624 | 1.603 | 0.624 |

| | | | | | | | |
|-------|----|-------|-------|-------|-------|-------|-------|
| Modal | 7 | 1.191 | 0.84 | 1.191 | 0.84 | 1.191 | 0.84 |
| Modal | 8 | 1.027 | 0.974 | 1.027 | 0.974 | 1.027 | 0.974 |
| Modal | 9 | 0.803 | 1.245 | 0.803 | 1.245 | 0.803 | 1.245 |
| Modal | 10 | 0.782 | 1.279 | 0.782 | 1.279 | 0.782 | 1.279 |
| Modal | 11 | 0.645 | 1.55 | 0.645 | 1.55 | 0.645 | 1.55 |
| Modal | 12 | 0.581 | 1.72 | 0.581 | 1.72 | 0.581 | 1.72 |

Mode 1 is having maximum time period of 6.298sec and 0.159 cyc/sec Frequency which is same for all three type of soils.

Mode shapes of shear wall

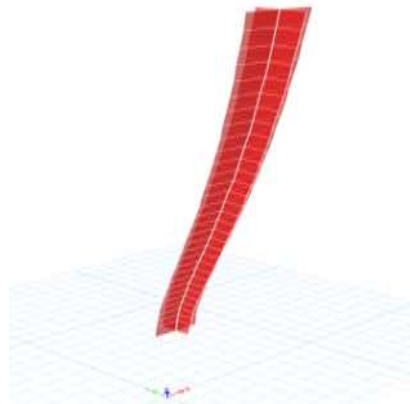


Figure 3: Mode shape 1 for shear wall

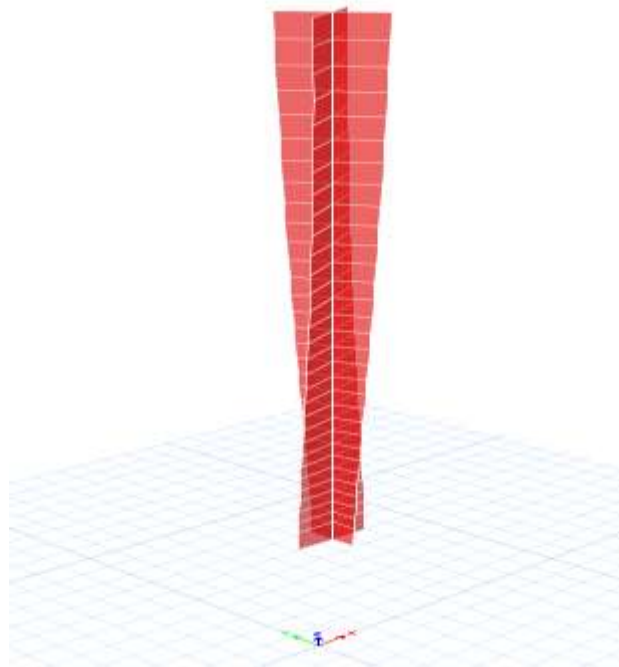


Figure 4: Mode shape 2 for shear wall

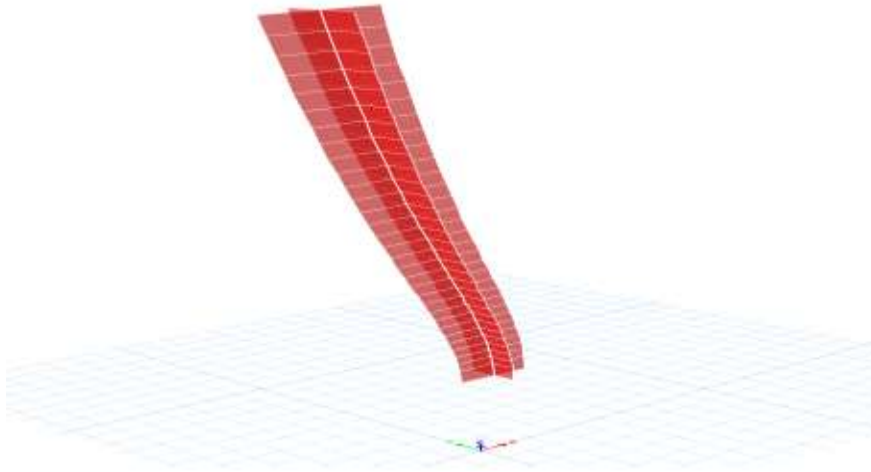


Figure 5: Mode shape 3 for shear wall

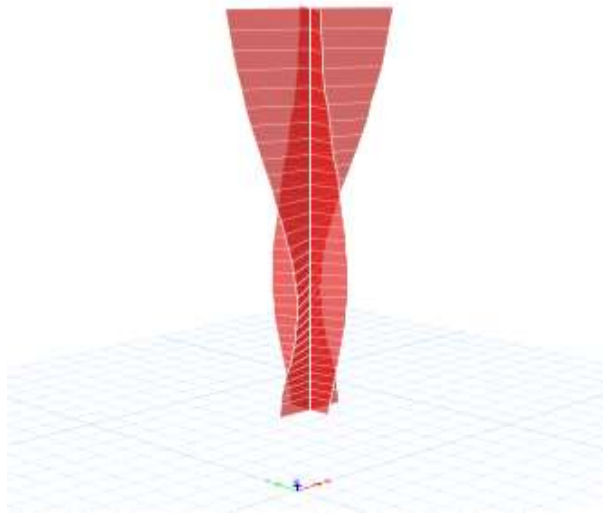


Figure 6: Mode shape 4 for shear wall

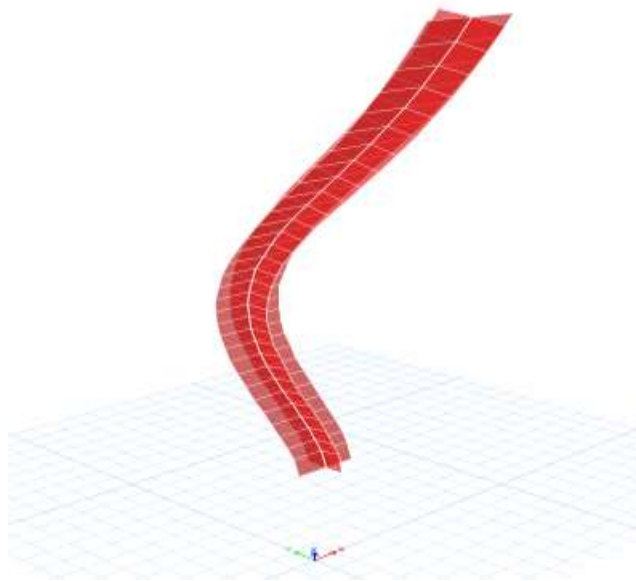


Figure 7: Mode shape 5 for shear wall

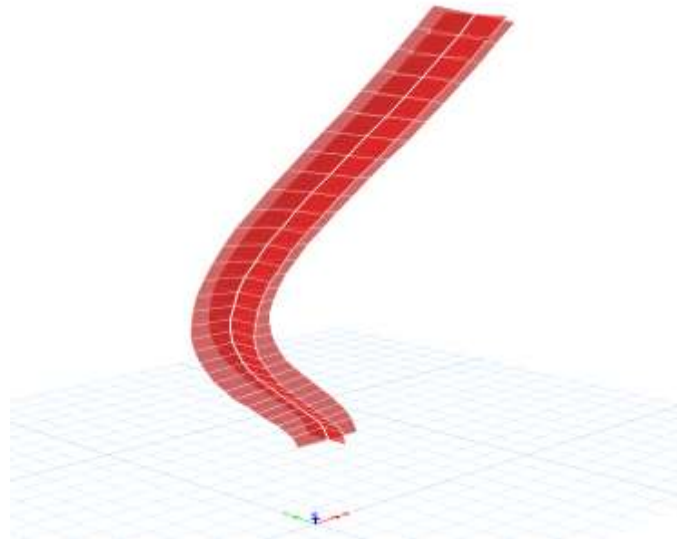


Figure 8: Mode shape6 for shear wall

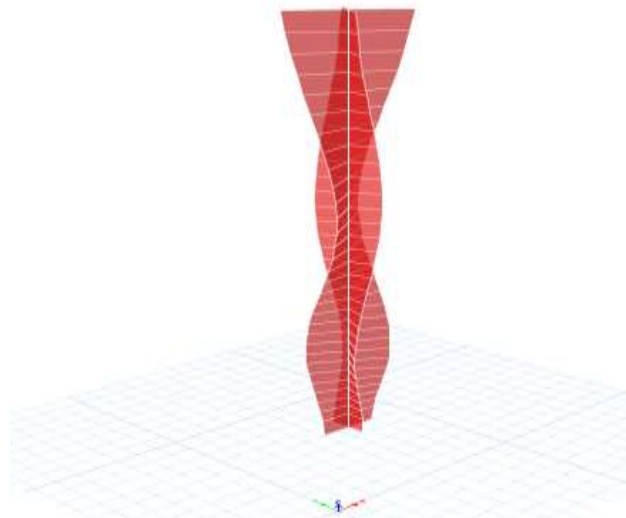


Figure 9: Mode shape 7 for shear wall

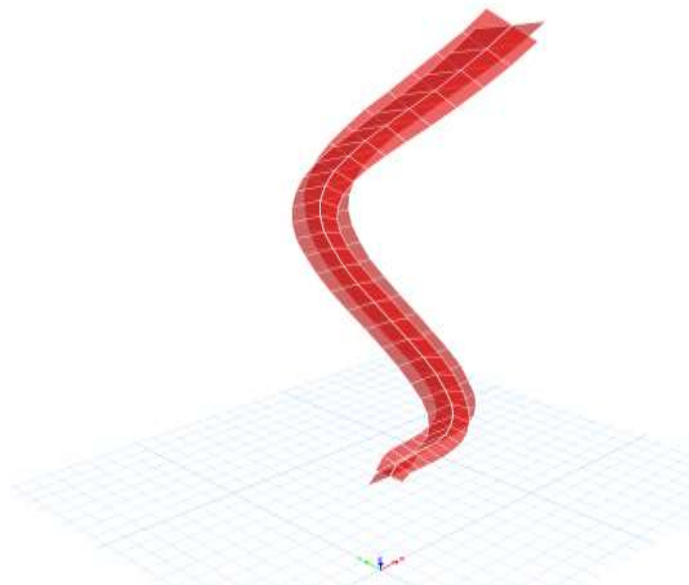


Figure 10: Mode shape 8 for shear wall

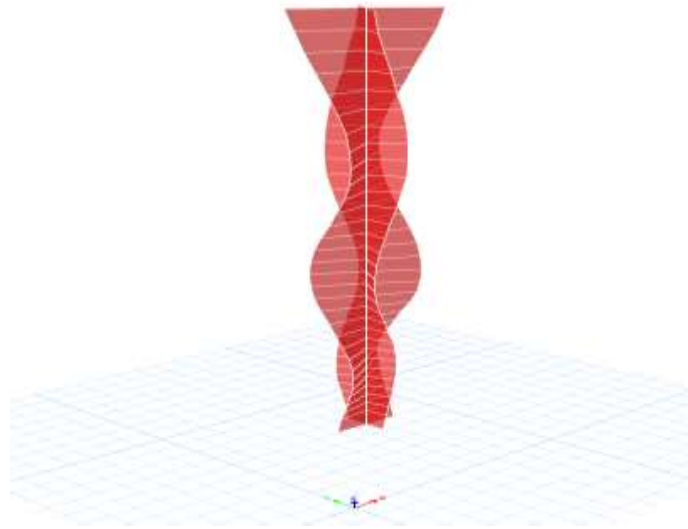


Figure 11: Mode shape 9 for shear wall

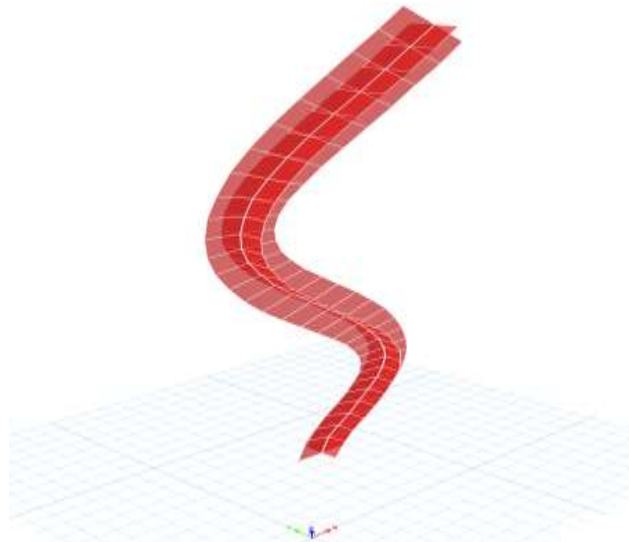


Figure 12: Mode shape 10 for shear wall

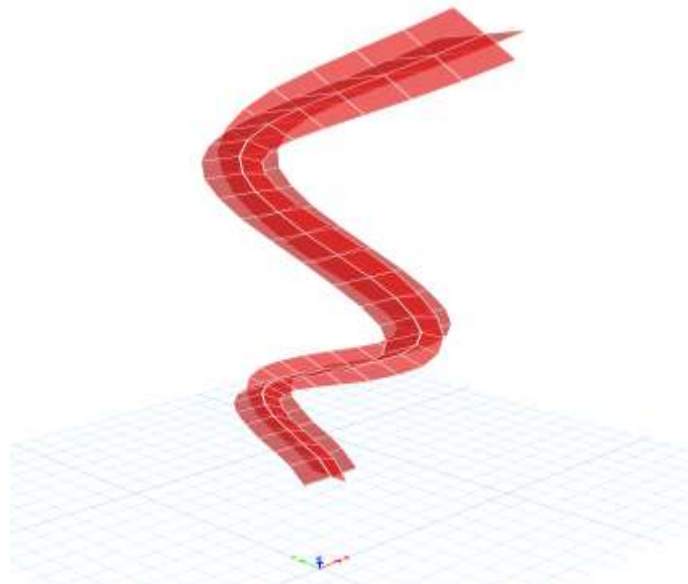


Figure 13: Mode shape 11 for shear wall

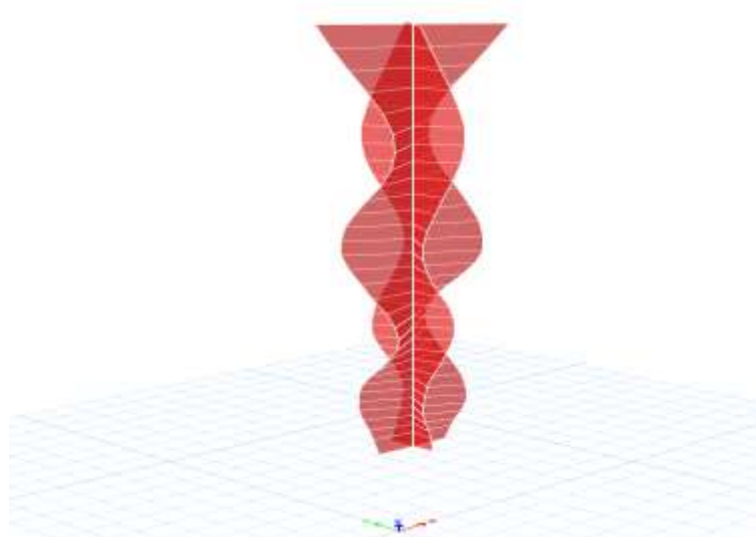


Figure 14: Mode shape 12 for shear wall

III. DISCUSSION ON RESULTS

The result obtained from the analysis models will be discussed and compared as follows:

It is observed that

- ❖ The time period is 6.298Sec for structure and it is same for different type of soil.
- ❖ The Frequency is 0.159cyc/sec and it is same for different type of soil.

It is observed that

- ❖ The percentage of displacement in X& Y direction is more by 35.94 % of the model in medium soil and 66.90 % of model in hard soil compared with model in soft soil.

It is observed that

- ❖ The maximum storey drift in X-direction occurred at storey 13th for the model in hard ,medium and soft soil.
- ❖ The percentage of storey drift in X- direction is decreased by placing shear wall as shown below :-
- ❖ 35.90 % of model in medium soil compared with model in soft soil.
- ❖ 66.79% of model in hard soil compared with model in soft soil.

It is observed that

- ❖ The maximum column axial force is various with type of soil and placing of the shear wall.column axial force in soft soil>medium soil>hard soil.

It is observed that

- ❖ The maximum column moment in Y-direction is influenced by the type of soil and placing of shear wall.
- ❖ The maximum column moment M2 in X-direction for soft Soil >Medium soil > Hard soil.
- ❖ The maximum column moment M3 in X-direction for soft Soil <Medium soil < Hard soil.
- ❖ The maximum column moment M2 in Y-direction for soft Soil <Medium soil < Hard soil.
- ❖ The maximum column moment M3in Y-direction for soft Soil >Medium soil > Hard soil.

It is observed that

- ❖ The maximum column Shear V2 in X-direction for soft Soil <Medium soil < Hard soil.
- ❖ The maximum column Shear V3 in X-direction for soft Soil >Medium soil > Hard soil.
- ❖ The maximum column Shear V2 in Y-direction for soft Soil>Medium soil > Hard soil.
- ❖ The maximum column Shear V3 in Y-direction for soft Soil <Medium soil < Hard soil.

It is observed that

- ❖ The maximum column Torsion , T in X-direction for soft Soil >Medium soil > Hard soil.
- ❖ The maximum column Torsion , T in Y-direction for soft Soil <Medium soil < Hard soil.

It is observed that

Shear Wall forces (Pier Forces)

- ❖ For the Pier axial forces in X direction There is not considerable difference for soft Soil ,Medium soil & Hard soil.
- ❖ Pier Moment M2 in X direction for soft soil <medium soil < hard soil .
- ❖ Pier Moment M3 in X direction for soft soil =medium soil = hard soil .
- ❖ Pier Moment M2 in Y direction for soft soil =Medium soil = hard soil .
- ❖ Pier Moment M3 in Y direction for soft soil <Medium soil < hard soil .
- ❖ Pier Shear Forces V2 in X direction for soft soil =Medium soil = hard soil.
- ❖ Pier Shear Forces V3 in X direction for soft soil >Medium soil > hard soil.
- ❖ Pier Torsion in X direction for soft soil >Medium soil > hard soil.
- ❖ Pier Torsion in Y direction for soft soil <Medium soil < hard soil.

It is observed that

- ❖ There is considerable difference in storey shear force in x-direction with a type of soils.
- ❖ The value of the storey shear force in x-direction decreases with increase in storey level.
- ❖ The value of the storey shear force in x-direction for the structure in soft soil is more compared with the structure in hard and medium soil.

It is observed that

- ❖ The value of the lateral loads in x-direction decreases with increase in storey level.
- ❖ The value of the lateral loads in x-direction for the structure in soft soil is less compared with the structure in medium soil and hard soil.
- ❖ lateral loads in X-direction for the structure in soft soil <Medium soil < hard soil.

It is observed that

- ❖ There is not difference in a storey moment in x-direction with a different type of soils.
- ❖ There is not difference in a storey moment in y-direction with a different type of soils.

It is observed that

- ❖ The value of the Stiffness of Structure in Soft Soil , Medium Soil and Hard Soil in X – direction for load cases EQXP is same .
- ❖ The value of the Stiffness of Structure in Soft Soil , Medium Soil and Hard Soil in Y – direction for load cases EQYP is same .

V. CONCLUSIONS

In this paper, reinforced concrete shear wall buildings were analyzed with the procedures laid out in IS codes. Seismic performance of building model is evaluated.

From the above results and discussions, following conclusions can be drawn:

- ❖ Shear Walls must be coinciding with the centroid of the building for better performance. It follows that a centre core Shear wall should be provided.
- ❖ The shear wall and its position has a significant influence on the time period. The time period is not influenced by the type of soil.
- ❖ Shear is affected marginally by placing of the shear wall, grouping of shear wall and type of soil. The shear is increased by adding shear wall due to increase the seismic weight of the building.
- ❖ Provision of the shear wall, generally results in reducing the displacement because the shear wall increases the stiffness of the building. The displacement is influenced by type and location of the shear wall and also by changing soil condition. The better performance for model with soft soil because it has low displacement.
- ❖ For both X and Y directions, the behaviour of the displacement graph is similar for model in Soft Soil , Medium Soil and Hard Soil. The order of maximum storey displacement in both the directions for the models is same.
- ❖ The shear force resisted by the column frame is decreasing by placing the shear wall and the shear force resisted by the shear wall is increasing. This can be concluded indirectly by observing the maximum column shear force and moment in both directions.

- ❖ As per code, the actual drift is less than permissible drift. The parallel arrangement of shear wall in the center core and outer periphery is giving very good result in controlling drift in both the direction. The better performance for model with soft soil because it has low storey drift.
- ❖ The moment resisting frame with shear walls are very good in lateral force such as earthquake and wind force. The shear walls provide lateral load distribution by transferring the wind and earthquake loads to the foundation. And also impact on the lateral stiffness of the system and also carries gravity loads.
- ❖ It is evident that shear walls which are provided from the foundation to the rooftop, are one of the excellent mean for providing earthquake resistant to multistory reinforced building with different type of soil.
- ❖ For the columns located away from the shear wall the Bending Moment is high and shear force is less when compared with the columns connected to the shear wall.
- ❖ Based on the analysis and discussion ,shear wall are very much suitable for resisting earthquake induced lateral forces in multistoried structural systems when compared to multistoried structural systems whit out shear walls. They can be made to behave in a ductile manner by adopting proper detailing techniques.
- ❖ The vertical reinforcement that is uniformly distributed in the shear wall shall not be less than the horizontal reinforcement .This provision is particularly for squat walls (i.e. Height-to-width ratio is about 1.0).However ,for walls whit height-to-width ratio less than 1.0, a major part of the shear force is resisted by the vertical reinforcement. Hence ,adequate vertical reinforcement should be provided for such walls.
- ❖ According to IS-1893:2002 the number of modes to be used in the analysis should be such that the total sum of modal masses of all modes considered is at least 90 percent of the total seismic mass. Here the minimum modal mass is 86.71 percent.
- ❖ It is observed that the column axial force is various with type of soil and placing of the shear wall.
- ❖ It is observed that the column shear force in x&ydirection is influenced by the type of soil and placing of the shear wall.
- ❖ It is observed that the column torsion is influenced by the type of soil and placing shear wall.
- ❖ It is observed that the column moment is influenced by the type of soil and placing of shear wall.
- ❖ It is observed that the Pier shear force is various with type of soil and placing of the shear wall.
- ❖ It is observed that the pier Torsion is various with type of soil and placing of the shear wall.
- ❖ It is observed that the There is not difference in a storey moment with a different type of soils.
- ❖ It is observed that the pier Moment is various with type of soil and placing of the shear wall
- ❖ It is observed that the There is not considerable difference in Pier Axial Force is various with type of soil and placing of the shear wall.
- ❖ It is observed that the value of stiffness in x& y-direction is same for the model with a different type of soil and placing shear wall.

REFERENCES

- [1]. Duggal, S.K., "Earthquake Resistant Design of Structures" Oxford University Press, New Delhi 2010
- [2]. Chopra, A.K., "Dynamics of Structures: Theory and Application to Earthquake Engineering", Pearson Education, 4th edition, 2012.
- [3]. Bureau of Indian Standards, IS 456 : 2000, "Plain and Reinforced Concrete-Code of practice", New Delhi, India.
- [4]. Bureau of Indian Standards: IS 13920 : 1993, "Ductile detailing of reinforced concrete structures subjected to seismic forces— Code of Practice", New Delhi, India.
- [5]. Bureau of Indian Standards: IS 875(part 1) : 1987, "Dead loads on buildings and Structures", New Delhi, India.
- [6]. Bureau of Indian Standards: IS 875(part 2) : 1987, "Live loads on buildings and Structures",New Delhi, India.
- [7]. Bureau of Indian Standards: IS 1893 (part 1) : 2002, "Criteria for earthquake resistant design of structures: Part 1 General provisions and buildings", New Delhi, India.
- [8]. Berkeley "ETABS Integrated Building Design Software", Computers and Structure, Inc., California, USA, February 2003
- [9]. Gary R.scarer and Sigmund A.Freeman " Design drifts requirement for long period structures ", 1 3 ' World conference on earth quake engineering Vancouver,B.C, Canada ,Aug 2004 paper no-3292 .
- [10]. J.L.Humar and S.Yavari "Design of concrete shear wall buildings for earthquake induced torsion". 4'1" structural conference of the Canadian society for civil engineering June-2002.
- [11]. Mo and Jost,"the seismic response of multistory reinforced concrete framed shear walls using a nonlinear model" , Volume 15, Structure Engineering , Issue 3, 1993, Pages 155–166 .
- [12]. Paulay,T., and Priestley, M.J.N., 'Seismic design of reinforced concrete and masonry buildings', 1992.
- [13]. Anand, N. ,Mightraj, C. and Prince Arulraj, G. "Seismic behaviour of RCC shear wall under different soil conditions" Indian geotechnical conference, Dec – 2010, pp 119-120.
- [14]. Anshuman, S., DipenduBhunia, BhavinRamjiyani,"Solution of shear wall location in multistory building", International journal of civil and structural engineering, Vol. 4, Issue 5, pp. 22-32 ,2011.
- [15]. Chandiwala, A., "Earthquake Analysis of Building Configuration withDifferent Position of Shear Wall", International Journal of Emerging Technology and Advanced Engineering ISSN 2250-2459, ISO 9001:2008 Certified Journal, Volume 2, Issue 12, December 2012
- [16]. Chandurkar, P.P., Dr. Pajgade, P.S., "Seismic analysis of RCC building with and without shear wall", International Journal of Modern Engineering Research. Vol. 3, Issue 3, pp. 1805-1810, 2013.
- [17]. Rahangdale, H., Satone, S.R., "Design and analysis of multi-storied building with effect of shear wall", International journal of engineering research and application", Vol. 3, Issue 3, pp. 223-232, 2013.