A Comprehensive Transmission Expansion Planning Strategy for Developing Countries

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Abstract—In the recent past, developing countries are moving into Electricity Deregulation. As Electric load demand raise, Transmission Expansion Planning must be developed in a suitable and appropriate way to provide reliable and quality power to the consumers. The objective of the paper is to present a Comprehensive Transmission Expansion Planning (CTEP) by considering physical and operational constraints like power balance, power flow limit on transmission lines, power generation limit, right-off-way and bus voltage phase angle limit. CTEP is proposed for Garver 6-bus system in view of contingencies like generator outage, line outage, combined generator and line outage, rise in load demand and rise in both generation and load demand. CTEP is proposed to achieve optimal planning cost, increased reliability and reduced transmission losses. AC load flow using Newton Raphson Method is considered for making CTEP in this paper.

Keywords—CTEP, right –off-way, optimal planning cost, reliability, Transmission losses and AC load flow

I. INTRODUCTION

Electrical energy is acceptable form of energy since it can be transported simply at high efficiency and sensible cost. Currently the Electrical Power Systems are large-scale and highly composite interconnected transmission systems. An electric power system can be subdivided into three major parts like generation, transmission and distribution. The principle of a transmission system is to transmit electrical energy from generating stations located at various places to the distribution systems and to ultimately provide supply to the load centers. Transmission system interconnects the adjacent utilities to allow economic dispatch of power across different areas during normal and emergency conditions.

In the recent past, the quantity of electrical power to be transferred from generating stations to major load centers has been rising significantly. Owing to mounting costs and the essential need for reliable electrical power systems, appropriate and best possible design methods for different parts of the power system are necessary. Transmission system occupies a major part of any power system, thus they have to be perfectly and efficiently planned [7]. Due to augmentation of power system, grid connected transmission lines have emerged, providing different paths for power flows from various generators to loads improving the reliability of continuous supply. Interconnection of transmission system removes the imbalance of generation and load by transmitting surplus power to the regions which are having deficiency of power. Supplementary transmission capability is necessary, whenever there is a need to transmit cheaper power to meet mounting load demand or improve system reliability or both.

II. OBJECTIVE OF TEP

The aim of Transmission Expansion Planning (TEP) is to specify addition of transmission lines that give sufficient power and at the same time maintain reliability of transmission system [3]. To congregate demand escalation, generation addition and augmented power flow, Transmission Expansion Planning must identify efficient plan, precise site, capacity, timing and type of novel transmission apparatus [3]. One of the major challenge in power system optimization is that TEP should be cost-effective in spite of the problem being complex, large-scale and nonlinear [5]. Planning horizon, instance topology of the base year, candidate circuits, load forecast, generation expansion and investment constraints are to be considered for TEP, increasing the complexity of the problem [3].

Comprehensive Transmission Expansion Planning (CTEP) shall be made based on analysis of AC load flow or DC load flow. Real and Reactive Power flows can be obtained from AC load flow or DC load flow [1]. In this paper AC load flow is considered in view of including transmission losses, but in DC load flow transmission losses are zero. CTEP can be computed by analyzing the line flows between whether they are exceeded or not and detailed analysis is as described in section 5.

III. PROBLEM STATEMENT

The TEP presents the problem of finding the finest number of transmission lines that must be added to an existing network to supply the forecasted load demand as economically as possible by considering operating constraints [5]. The physical and economical constraints are to be considered in the TEP to minimize the capital and operating costs of the electrical transmission network [3]. The constraints are very vital while attempting to develop a power system at a lowest cost considering fiscal and load restrictions that placed upon the system [7]. The TEP problem can be defined in the following manner [3]:

 $\min \nu = \sum_{i=1}^{NB} \sum_{j=1}^{NB} C_{ij} n_{ij} + K \sum_{i=1}^{NL} I_i^2 R_i$ (1)

Cii- Cost of the new transmission line added to line i-j

n_{ii}- Number of transmission lines added to the line i-j

NB- Total number of buses

K- Loss coefficient, K=8760*NYE*CkWh

NYE- Anticipated life span of the Transmission Expansion Network in years

CkWh- Cost of one kWh in \$/kWh

R_i- Resistance of the ith line

I_i- Current through ith line

NL- Number of present transmission lines

The loss coefficient (K) relies on the number of years of operation and the cost of kWh i.e. cost of kWh increases with number of years of operation that leads to rise in loss coefficient [4].

The TEP problem (1) represents the capital cost of the recently installed transmission lines, it has some restrictions to solve it. To find optimal solution of TEP, physical and operational constraints must be included into the mathematical model. The constraints are explained as follows [7]:

3.1 Power Flow Node Balance

The non linear equality constraint represents the conservation of power at each node, i.e.

 $P_{Gi} = P_{Di} + P_i$ (2) for i=1, 2NB

Where P_{Gi}, P_{Di} and P_i is real power generation, real load demand and real power injection at bus i, respectively.

3.2 Power Flow Limit On Transmission Lines

The inequality constraint of power flow limit on transmission line for each path is $\left|P_{ij}\right| \leq \left(n_{ij}^{0} + n_{ij}\right)P_{ij}^{max}$ (3)Where P_{ii} , P_{ii}^{max} , n_{ii} and n_{ii}^{0} gives total power flow through transmission line i-j, maximum power flow through transmission line i-j, number of lines added to transmission line i-j and number of transmission lines in original base system, respectively.

3.3 Power Generation Limit

In TEP, power generation limit should be incorporated as one of the constraints. Mathematically, it can be represented as follows:

 $P_{gi}^{min} \le P_{gi} \le P_{gi}^{max}$ (4) Where P_{gi} , P_{gi}^{min} and P_{gi}^{max} is real power generation at bus I, the lower and upper real power generation bounds at bus i, respectively.

3.4 Right Of Way

The planners need to know the exact location and capacity of the newly required transmission lines for a precise TEP. Hence this constraint should be incorporated into the deliberation of planning problem. The new transmission line location and the maximum number of lines that can be installed in a specified location shall be obtained from this constraint, it can be represented mathematically as follows:

$$0 \le n_{ij} \le n_{ij}^{max} \tag{5}$$

Where n_{ij} and n_{ij}^{max} is the total number of lines added to the transmission line i-j and the maximum number of added lines in the transmission line i-j, respectively.

3.5 Bus Voltage Phase Angle Limit

The bus voltage phase angle is incorporated as a TEP constraint and the calculated voltage phase angle (θ_i^{cal}) must be less than the specified maximum voltage phase angle (θ_i^{max}), it can be defined mathematically as: $\left|\theta_{i}^{cal}\right| \leq \left|\theta_{i}^{max}\right|$

To check the reliability of the transmission system, the TEP problem should not only consider the usual operation but also incorporate contingencies due to changes in the system, e.g., generator outage, line outage, load uncertainties, etc.

3.6 Generator Outage

Generating capacity may be reduced by declaring a "forced outage" to make repairs, or by extending a planned outage for maintenance. Reducing generating capacity may be lead to an artificial shortage of electricity supply and create reliability problems. Due to internal or external faults of generators, generator outage may be happened, hence this constraint should be included in TEP problem.

3.7 Transmission Line Outage

The main reasons of transmission line outages are adverse weather (i.e. due to lighting, wind and icing), faulty equipment, foreign intervention, bad environment, and human element, it leads to interruption of power supply, hence this constraint must be incorporated in TEP problem.

3.8 Load Uncertainties

The reasons for uncertainty in load are, that the load is always variable, future load is a random variable, random results may be produced by load forecasting methods, errors in forecasted result and the majority of methods suffer from missing data and input data accuracy. Hence, this constraint must be integrated in TEP problem.

IV. AC LOAD FLOW

Load flow analysis gives steady state information about bus voltages, current injections at all buses, real and reactive power flows through transmission lines for given power system. The representation of AC load flow can be illustrated by the equations given below:

$$P_{i} = \sum_{k=1}^{n} |V_{i}||V_{k}||Y_{ik}| \cos(\theta_{ik} + \delta_{k} - \delta_{i})$$
(7)
$$Q_{i} = -\sum_{k=1}^{n} |V_{i}||V_{k}||Y_{ik}| \sin(\theta_{ik} + \delta_{k} - \delta_{i})$$
(8)

For i=1, 2...NB and k=1, 2...NB

Where P_i , Q_i , $|V_i|$, θ_{ik} , δ_i and δ_k is real power injection, reactive power injection, voltage magnitude at bus i, admittance angle of line i-k, voltage phase angle at bus i and voltage phase angle at bus k, respectively.

In this paper, to solve AC load flow, Newton-Raphson (NR) method [1] is considered. The following steps are involved in solving AC load flow using NR method [1]:

i. Reading the bus data, line data, initial guess and convergence criteria.

- ii. Forming the bus admittance matrix.
- iii. Setting the bus count i=2 and iteration count r=0.
- iv. Testing the type of bus, If bus is PQ bus, find P_i^r and Q_i^r using equation (7) and (8) respectively and also find $\Delta P_i^r = P_{i \ specified} P_i^r$ and $\Delta Q_i^r = Q_{i \ specified} Q_i^r$. If bus is PV bus, calculate P_i^r and Q_i^r using equation (7) and (8) respectively and also determine $\Delta P_i^r = P_{i \ specified} P_i^r$.
- v. Advancing the bus count $i \rightarrow i + 1$ and if i < n, go to step iv and otherwise go to step vi.
- vi. Checking the change in power i.e. to verify whether $\Delta P_i^r \leq \epsilon$ and $\Delta Q_i^r \leq \epsilon$ are satisfied or not. If this condition is satisfied, go to step xi and otherwise go to step vii to find Jacobian Matrix.
- vii. Computing the elements of Jacobian Matrix 'J'.
- viii. Calculating the change in voltage magnitudes and phase angles using P_i^r , Q_i^r and J.
- ix. Updating the voltage magnitudes and phase angles and then go to step x.
- x. Advancing the iteration count $r \rightarrow r + 1$ and then go to step iv.
- xi. Computing the slack bus powers and line flows.
- xii. Printing the results and stop the iteration.

V. CTEP USING AC LOAD FLOW

CTEP can be made using AC load flow analysis, since it gives real and reactive power flows and line flows. The steps involved in CTEP using AC load flow by considering constraints as explained in section 3, are explained as follows:

- i. Reading the bus data, line data, initial guess, convergence criteria and constraints involved in CTEP.
- ii. Executing the AC load flow using NR Method.
- iii. Checking the power balance equation is satisfied or not. If it is satisfied, go to step v, otherwise transmit power from other areas to balance the load or go for load shedding to balance the load.
- iv. Testing the generating power is within the specified limits or not. If it exceeds the maximum limit, reduce load on that generator and if it exceeds the minimum limit stop the generator.
- v. Verifying the line flows are within the limits or not. If line flows exceeded the specified line flow limit, find which line has highest exceeded line flow then add a line across it and go to step ii to run AC load flow, otherwise go to step vi.
- vi. Checking the number of lines between any two buses exceeded right off way limit or not. If it is exceeded, remove the line and go to step ii, otherwise go to step vii.
- vii. If there is generator outage, go to step ii, otherwise go to step viii.
- viii. If there is line outage, go to step ii, otherwise go to step ix.
- ix. If there is load uncertainty, go to step ii, otherwise go to step x.
- x. Printing the results and find the cost required for adding new transmission lines.

VI. RESULTS & DISCUSSION

In this paper Garver 6-bus system is taken as case study. Single line diagram of Garver 6-bus system is shown in figure 1. Comprehensive Transmission Expansion Planning (CTEP) is done based on optimum expansion cost, reliable operation and reducing transmission losses by satisfying the physical and operational constraints from 3.1 to 3.5 as explained in section 3. Generation and load data and Branch data represented in table 1 and table 2 respectively. CTEP using AC Load Flow is explained in section 5. CTEP is made for the following contingencies in this paper.

- i. Normal Operation
- ii. Generator Outage
- iii. Line Outage
- iv. Both Generator and Line Outage

- v. Change in Load Demand
- vi. Change in both Generation and Load Demand

Detailed analysis of CTEP for above mentioned contingencies is explained as follows:

6.1: Normal Operation:

In this case total load on the system is 760MW, maximum available generation is 1110MW and lines 1-2, 1-4, 1-5, 2-3, 2-4 and 3-5 are connected to the system. Before CTEP, under normal operating mode, some of the physical constraints are not satisfied. All the constraints are satisfied after completion of CTEP. In this case new lines added are $n_{2-6}=2$, $n_{3-5}=2$ & $n_{4-6}=2$, Transmission Expansion cost is 160×10^3 US\$, losses are 30.36MW and load shedding is not taken place.

6.2: Generator Outage:

There are three generators in the system. Here CTEP is studied for single generator outage and double generator outage. Detailed analysis of CTEP for generator outage is explained below:

6.2.1: Outage of Generator 1:

When generator 1 is in outage, CTEP is done by satisfying all the constraints. For this mode, new lines added are $n_{2-6}=3$, $n_{3-5}=2 \& n_{4-6}=2$, expansion cost is 190x10³ US\$, losses are 56.24MW and load shedding is not made.

6.2.2: Outage of Generator 2:

In case of outage of generator 2, CTEP is accomplished in fulfilling all the constraints. In this mode, new lines included are $n_{2-6}=3$, $n_{3-5}=2$ & $n_{4-6}=2$, extension cost is 250x10³ US\$, losses are 43.55MW and 60MW of load is gone for shedding.

6.2.3: Outage of Generator 3:

While generator 3 is outage state, CTEP is prepared by satisfying all the constraints. In this case, new lines incorporated are $n_{2-3}=1 \& n_{3-5}=1$, lines addition cost is 40x10³ US\$, losses are 32.14MW and 285MW of load is left for shedding.

6.2.4: Outage of Generator 1 and Generator 2:

If both the generator 1 and 2 are in outage, CTEP is completed via gratifying all the constraints. For this approach, new lines integrated are $n_{2-6}=4$, $n_{4-6}=2$ & $n_{5-6}=2$, expansion cost is 302×10^3 US\$, losses are 55.97MW and 216.5MW of load is gone for shedding.

6.3: Line Outage:

Presently Garver 6-bus system has 6 lines. In this case CTEP is discussed for single line outages. Thorough analysis of CTEP for line outage is enlightened as follows:

6.3.1: Outage of Line 1-2:

CTEP is made by satisfying all the constraints for outage of line 1-2. For this mode, new lines added are $n_{2-3}=1$, $n_{2-6}=1$, $n_{3-5}=1$, $n_{3-6}=1$ & $n_{4-6}=2$, expansion cost is 170x10³ US\$, losses are 35.68MW and load shedding is not made.

6.3.2: Outage of Line 1-4:

CTEP is accomplished in fulfilling all the constraints for outage of line 1-4. In this mode, new lines included are $n_{2-3}=1$, $n_{2-6}=2$, $n_{3-5}=2$, & $n_{4-6}=2$, extension cost is 180x10³ US\$, losses are 27.84MW and no load is gone for shedding.

6.3.3: Outage of Line 1-5:

CTEP is prepared by satisfying all the constraints for outage of line 1-5. In this case, new lines incorporated are $n_{2.6}=2$, $n_{3.5}=2 \& n_{4.6}=2$, lines addition cost is 160×10^3 US\$, losses are 32.06MW and load shedding is not taken place.

6.3.4: Outage of Line 2-3:

CTEP is completed via gratifying all the constraints when line 2-3 is gone for outage. For this approach, new lines integrated are $n_{2-6}=2$, $n_{3-5}=2$, $n_{3-6}=1$ & $n_{4-6}=2$, expansion cost is 200x10³ US\$, losses are 43.53MW and 216.5MW of load is gone for shedding.

6.3.5: Outage of Line 2-4:

CTEP is finished through satisfying all the constraints while line 2-4 is left for outage. For this mode, new lines included are $n_{2-6}=2$, $n_{3-5}=2$, $n_{3-6}=1$ & $n_{4-6}=2$, expansion cost is 160×10^3 US\$, losses are 30.49MW and load shedding is 0.

6.3.6: Outage of Line 3-5:

CTEP is done by satisfying all the constraints while line 2-4 is left for outage. For this case, new lines incorporated are $n_{2-6}=2$, $n_{3-5}=2$, $n_{3-6}=1$ & $n_{4-6}=2$, expansion cost is 230x10³ US\$, losses are 65.38MW and load shedding is mot made.

6.4: Both Generator and Line Outage:

Combination of generator and line outages are considered in this approach. CTEP is made for both generator and line outages by fulfilling all the constraints and scrupulous study is explained as follows:

6.4.1: Outage of Generator 1 and Line 1-2:

In case of CTEP for outage of generator 1 and line 1-2, new lines added are $n_{2-6}=3$, $n_{3-5}=2$ & $n_{4-6}=3$, expansion cost is 220×10^3 US\$, losses are 45.02MW and load shedding is not made.

6.4.2: Outage of Generator 1 and Line 1-4:

In view of CTEP for outage of generator 1 and line 1-4, new lines included are $n_{2-6}=3$, $n_{3-5}=2$ & $n_{4-6}=2$, extension cost is 190×10^3 US\$, losses are 50.93MW and no load is gone for shedding.

6.4.3: Outage of Generator 1 and Line 1-5:

Since CTEP for outage of generator 1 and line 1-5, new lines incorporated are $n_{2-6}=4$, $n_{3-5}=2$ & $n_{4-6}=2$, lines addition cost is 220×10^3 US\$, losses are 45.44MW and load shedding is not taken place.

6.4.4: Outage of Generator 2 and Line 2-3:

While CTEP for outage of generator 2 and line 2-3, new lines integrated are $n_{2-6}=3$, $n_{3-5}=1$, $n_{3-6}=2$ & $n_{4-6}=2$, expansion cost is 250x10³ US\$, losses are 42.05MW and 60MW of load is gone for shedding.

6.4.5: Outage of Generator 2 and Line 3-5:

In view of CTEP for outage of generator 2 and line 3-5, new lines included are $n_{1-2}=1$, $n_{1-5}=2$, $n_{2-6}=4$ & $n_{4-6}=3$, expansion cost is 290x10³ US\$, losses are 60.35MW and 75MW of load is left for shedding.

6.5: Change in Load Demand:

In the developing countries like India, there will be around 10% load growth per year. In this case, 10%, 20% and 30% load growth is considered, then CTEP is prepared by satisfying all the constraints and thorough study is explained as follows:

6.5.1: 10% Rise in Load Demand:

CTEP is made for 10% rise in load demand, then new lines added are $n_{2.6}=2$, $n_{3.5}=2$ & $n_{4.6}=2$, expansion cost is 160×10^3 US\$, losses are 42.06MW and load shedding is not made.

6.5.2: 20% Rise in Load demand:

CTEP is prepared for 20% rise in load demand, then new lines included are $n_{2-6}=3$, $n_{3-5}=2$ & $n_{4-6}=2$, extension cost is 190×10^3 US\$, losses are 48.71MW and no load is gone for shedding.

6.5.3: 30% Rise in Load demand:

CTEP is accomplished for 30% rise in load demand, then new lines incorporated are $n_{2-6}=4$, $n_{3-5}=2$ & $n_{4-6}=3$, lines addition cost is 250x10³ US\$, losses are 50.46MW and load shedding is not taken place.

6.6: Change in both Generation and Load Demand:

In the developing countries like India, there will be around 10% load growth per year and consequently grow in Generation on par with increase in load. In this mode, 10%, 20% and 30% rise in both generation and load is considered, then CTEP is accomplished by fulfilling all the constraints and detailed study is explained as follows:

6.6.1: 10% Rise in Generation and Load Demand:

In view of CTEP for 10% rise in Generation and load demand, then new lines added are $n_{2-3}=1$, $n_{2-6}=2$, $n_{3-5}=2$ & $n_{4-6}=2$, expansion cost is 180x10³ US\$, losses are 33.71MW and load shedding is not made.

6.6.2: 20% Rise in Generation and Load demand:

In case of CTEP for 20% rise in Generation and load demand, then new lines included are $n_{2-3}=1$, $n_{2-6}=2$, $n_{3-5}=2$ & $n_{4-6}=2$, extension cost is 180×10^3 US\$, losses are 42.35MW and no load is gone for shedding.

6.6.3: 30% Rise in Generation and Load demand:

Since CTEP for 30% rise in Generation and load demand, then new lines incorporated are $n_{2-3}=1$, $n_{2-6}=2$, $n_{3-5}=2$ & $n_{4-6}=3$, lines addition cost is 210x10³ US\$, losses are 44.38MW and load shedding is not taken place.

6.7: 10% Rise in Generation with Normal Operation:

CTEP is prepared for 10% rise in Generation with normal operation, new lines integrated are $n_{2-3}=1$, $n_{2-6}=1$, $n_{3-5}=2$ & $n_{4-6}=2$, expansion cost is 150×10^3 US\$, losses are 28.38MW and there is no load shedding. Table 3 represents CTEP for all type of contingencies mentioned in this paper.



Bus No	Generation (MW)		Lood (MW)				
	Maximum	Level	Load (MW)				
1	150	50	80				
2	0	0	240				
3	360	165	40				
4	0	0	160				
5	0	0	240				
6	600	545	0				
Table 1: Generation and Load data for Garver 6-bus system							

From – To	$\mathbf{n_{ij}}^{0}$	Resistance r _{ij} (pu)	Reactance x _{ii} (pu)	f_{ij}^{max} (MW)	Cost x 10 ³ US\$
1-2	1	0.1	0.4	100	40
1-3	0	0.09	0.38	100	40
1-4	1	0.15	0.6	80	60
1-5	1	0.05	0.2	100	20
1-6	0	0.17	0.68	70	50
2-3	1	0.05	0.2	100	20
2-4	1	0.1	0.4	100	40
2-5	0	0.08	0.31	100	20
2-6	0	0.08	0.3	100	30
3-4	0	0.15	0.59	82	60
3-5	1	0.05	0.2	100	20
3-6	0	0.012	0.48	100	40
4-5	0	0.16	0.63	75	50
4-6	0	0.08	0.3	100	30
5-6	0	0.15	0.61	78	61

Table 2: Branch data for Garver 6-bus system

S.No	Type of Contingency	New lines Added	Transmission Expansion Cost (X10 ³ \$)	Amount of Load Shedding (MW)	Transmission Losses (MW)
1	Normal Operation	$n_{2-6}=2, n_{3-5}=2 \& n_{4-6}=2$	160	0	30.36
2	Generator 1 outage	$n_{2-6}=3, n_{3-5}=2 \& n_{4-6}=2$	190	0	56.24
3	Generator 2 outage	$n_{2-6}=3, n_{3-5}=2 \& n_{4-6}=2$	250	60	43.55
4	Generator 3 outage	$n_{2-3}=1 \& n_{3-5}=1$	40	285	32.14
5	Generator 1 & 2 Outage	$n_{2-6}=4, n_{4-6}=2 \& n_{5-6}=2$	302	216.5	55.97
6	Line 1-2 Outage	$\begin{array}{c} n_{2\text{-}3} \! = \! 1, n_{2\text{-}6} \! = \! 1, n_{3\text{-}5} \! = \! 1 \ , \\ n_{3\text{-}6} \! = \! 1 \ \& \ n_{4\text{-}6} \! = \! 2 \end{array}$	170	0	35.68
7	Line 1-4 Outage	$\begin{array}{c} n_{2\text{-}3} \!\!=\!\! 1, n_{2\text{-}6} \!\!=\!\! 2, n_{3\text{-}5} \!\!=\!\! 2 \;, \\ \& n_{4\text{-}6} \!\!=\!\! 2 \end{array}$	180	0	27.84
8	Line 1-5 Outage	$n_{2-6}=2, n_{3-5}=2 \& n_{4-6}=2$	160	0	32.06
9	Line 2-3 Outage	$n_{2-6}=2, n_{3-5}=2, n_{3-6}=1$ & $n_{4-6}=2$	200	0	43.53
10	Line 2-4 Outage	$n_{2-6}=2, n_{3-5}=2 \& n_{4-6}=2$	160	0	30.49
11	Line 3-5 Outage	$n_{1-2}=1, n_{1-5}=2, n_{2-3}=3, n_{2-6}=1 \& n_{4-6}=2$	230	0	65.38
12	Gen 1 and line 1-2 Outage	n ₂₋₆ =3, n ₃₋₅ =2 & n ₄₋₆ =3	220	0	45.02
13	Gen 1 and line 1-4 Outage	$n_{2-6}=3, n_{3-5}=2 \& n_{4-6}=2$	190	0	50.93
14	Gen 1 and line 1-5 Outage	$n_{2-6}=4, n_{3-5}=2 \& n_{4-6}=2$	220	0	45.44
15	Gen 2 and line 2-3 Outage	$\begin{array}{c} n_{2\text{-}6}{=}3,n_{3\text{-}5}{=}1$, $n_{3\text{-}6}{=}2\\ \& n_{4\text{-}6}{=}2 \end{array}$	250	60	42.05
16	Gen 2 and line 3-5 Outage	$n_{1-2}=1, n_{1-5}=2, n_{2-6}=4$ & $n_{4-6}=3$	290	75	60.39
17	10% Rise in load demand	$n_{2-6}=2, n_{3-5}=2 \& n_{4-6}=2$	160	0	42.06
18	20% Rise in load demand	$n_{2-6}=3, n_{3-5}=2 \& n_{4-6}=2$	190	0	48.71
19	30% Rise in load demand	$n_{2-6}=4, n_{3-5}=2 \& n_{4-6}=3$	250	0	50.46
20	10% Rise in load & gen.	$\begin{array}{c} n_{2\text{-}3} = 1, n_{2\text{-}6} = 2, n_{3\text{-}5} = 2 \ , \\ \& n_{4\text{-}6} = 2 \end{array}$	180	0	33.71
21	20% Rise in load & gen.	$\begin{array}{c} n_{2\text{-}3} = 1, n_{2\text{-}6} = 2, n_{3\text{-}5} = 2 \;, \\ \& n_{4\text{-}6} = 2 \end{array}$	180	0	42.35
22	30% Rise in load & gen.	$\begin{array}{c} n_{2\text{-}3} = 1, n_{2\text{-}6} = 2, n_{3\text{-}5} = 2 \;, \\ \& n_{4\text{-}6} = 3 \end{array}$	210	0	44.38
23	Normal Operation with 10% rise in generation	$\begin{array}{c} n_{2\text{-}3}\!\!=\!\!1,n_{2\text{-}6}\!\!=\!\!1,n_{3\text{-}5}\!\!=\!\!2\;,\\ \& n_{4\text{-}6}\!\!=\!\!2 \end{array}$	150	0	28.38

Table 3: CTEP for Garver 6-bus system for different contingencies

VII. CONCLUSION

Comprehensive Transmission Expansion Planning (CTEP) is proposed for Garver 6-bus system. CTEP is completed by considering physical and operational constraints to achieve optimal transmission planning cost, reliability and reduced transmission losses. CTEP is developed for contingencies like generator outage, line outage, combined generator and line outage, rise in load demand and rise in both generation and load demand. CTEP for Garver 6-bus system for different contingencies is shown in Table 3. In this paper, optimal transmission cost, reliability and reduced transmission losses are achieved using CTEP for a Garver 6-bus system.

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