

# Digitally Programmable Voltage Mode Quadrature Oscillator Using Current Conveyors

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**Abstract:-** A simple technique is presented to realize a digitally programmable voltage mode quadrature oscillator using second generation current conveyors. Firstly, the current conveyors based tunable quadrature oscillator is realised. A digital block is introduced in the realized tunable quadrature oscillator so that the oscillator can be controlled digitally. The realized Digitally Programmable Quadrature oscillators enjoys attractive features such as use of low components count, independent digital control to frequency of oscillation and low sensitivity figures. The realized digitally programmable quadrature oscillator circuits are designed and verified with attractive results.

**Keywords:-** Current conveyors, Voltage-mode circuits, quadrature oscillators.

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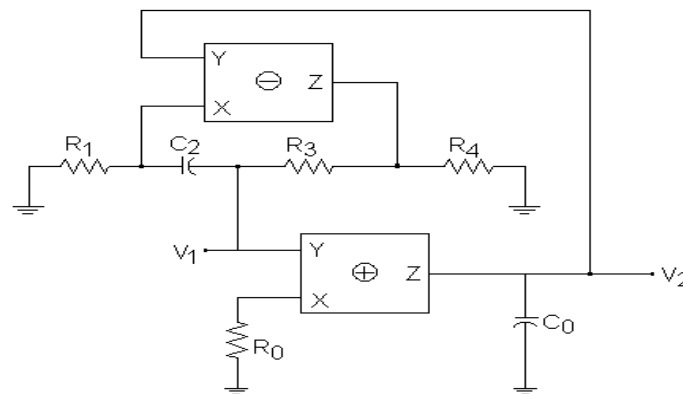
## I. INTRODUCTION

The current conveyors, introduced in 1968, is an extremely powerful analogue building block, combining voltage and current-mode capability. It possess higher signal bandwidth, greater linearity and large dynamic range. It has proved to be functionally flexible and versatile, rapidly gaining acceptance as a practical device with a wide range of high performance circuit and system application [1]-[2]. And the use of grounded resistors and capacitors is beneficial from the point of view of IC fabrication.

The sinusoidal quadrature oscillator find wide applications in instrumentation and communication systems. As a result several circuits using various active devices have been reported in technical literature [3]-[14]. In this paper a sinusoidal quadrature oscillator has been proposed using current conveyor as a basic building block. For the realization of digitally programmable quadrature oscillator (DPQO). Firstly a tunable quadrature oscillator using two current conveyors, three grounded resistors, one grounded capacitor and one floating resistor and capacitor, is realized. Secondly, digital block is introduced in the realized tunable quadrature oscillator so that it can be controlled digitally. So the realized oscillator provides wide adjustment range through digital control word, high resolution capability and complete reconfigure ability. The working ability of the oscillator has been confirmed by SPICE Simulation.

## II. QUADRATURE OSCILLATOR

The quadrature oscillator is given in Figure 1. It uses two CCII's, four resistors and two capacitors where  $R_0$ ,  $R_1$ ,  $R_3$  and  $C_0$  are in grounded form. For digital control the grounded resistors and capacitors can be replaced by the digitally programmable impedance multiplier, according to the requirement.



**Fig.1:** Tunable quadrature oscillator.

The routine analysis of the circuit gives the characteristic equation

$$s^2 + s \left( \frac{1}{R_2 C_1} - \frac{1}{R_0 C_0} \right) + \left( \frac{R_3 / R_1}{R_0 C_0 R_2 C_1} \right) = 0 \quad (1)$$

Which results in the condition of oscillation as

$$C_0 R_0 = R_2 C_1 \quad (2)$$

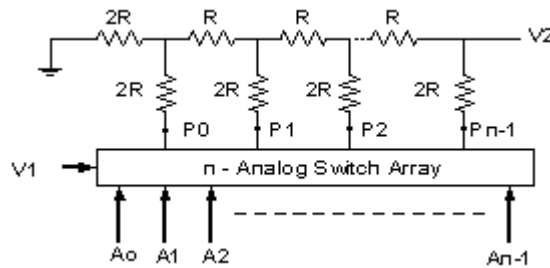
and frequency of Oscillation as

$$\omega_0 = \left( \frac{R_3 / R_1}{R_0 C_0 R_2 C_1} \right)^{\frac{1}{2}} \quad (3)$$

For the digital control of the realised tunable quadrature oscillator, the grounded resistor or capacitor can be replaced by digitally programmable impedance multiplier, as per the requirement. For digital control, the digital module of reference [3] is used.

### III. DIGITAL CONTROL MODULE

The realization of the digital control module(DCM) used in the DPGIM is shown in Figure 1(a), which uses R-2R ladder and analog switching array [6].



**Fig. 2(a): Digital Control Module- DCM.**

Its routine analysis yields the output voltage  $V_2$  as

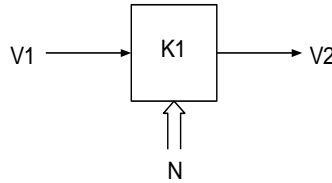
$$V_2 = \frac{V_1}{2^n} (A_0 + 2A_1 + 4A_2 + \dots + 2^{n-1} A_{n-1}) \quad (4)$$

Where,  $A_0, A_1, \dots, A_{n-1}$  are the bit values of the n-bit digital control word (N). Equation (1) can also be expressed as

$$V_2 = K_1 V_1 \quad (5)$$

where,  $K_1 = N/2^n$ .

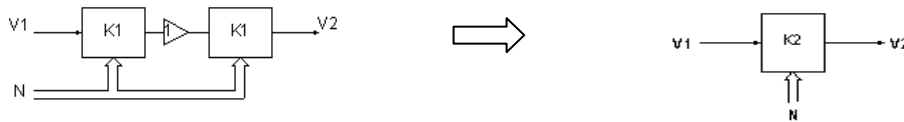
The equivalent of the Figure 2(a) is given in Figure 2(b) and now onwards shall be expressed as the  $K_1$ -Block. If two stages of the  $K_1$ -Block with same control word are cascaded through a voltage buffer as shown in Figure 2(c),



**Fig. 2(b): The  $K_1$  – Block.**

the transfer gain can be expressed as

$$\frac{V_2}{V_1} = K_2 \quad (6)$$



**Fig. 2(c): The  $K_2$  – Block**

Where,  $K_2 = K_1 K_1 = (N/2^n)^2$ . Henceforth, this double stage block shall be referred as the  $K_2$  – Block. Its equivalent is also shown in Figure 2(c). It is obvious from equation (5) and (6) that the transfer gain of the  $K_1$  and  $K_2$  modules can be controlled through digital control word (N)

**IV. DIGITALLY PROGRAMMABLE RESISTANCE MULTIPLIERS (DPRM)**

The basic scheme for realizing digitally programmable impedance multiplier (DPIM) reference [14]-[15] is shown in Figure 3. It uses one CCII, one digital control module of Figure 1, and the grounded impedance(Z) under control.

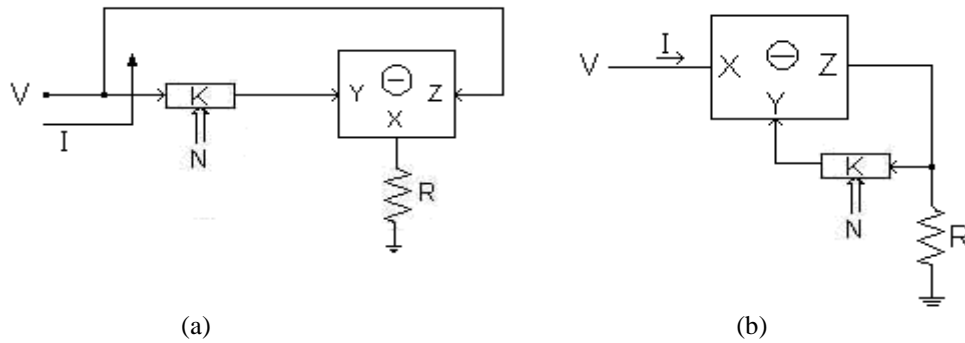


Fig. 3: Digitally programmable impedance multipliers

The routine analysis for DPIM of Figure 3(a) and Figure 3(b) yields the input impedance function respectively as

$$Z_{in} = \frac{V}{I} = \frac{R}{K} \tag{7a}$$

$$Z_{in} = \frac{V}{I} = KR \tag{7b}$$

where,  $K = \frac{N}{2^n}$ . It is to be noted that K-block input is to be buffered and K-block can be  $K_1$  or  $K_2$  block as per requirement.

**V. DIGITALLY PROGRAMMABLE QUADRATURE OSCILLATOR**

For the realization of digitally programmable quadrature oscillator, the DPRM of section 2 can be substituted in place of grounded resistors.

**Case I : Digitally Programmable Quadrature Oscillator 1 (DPQO1)**

For realizing DPQO1, the two resistances  $R_3$  and  $R_1$  will be replaced by DPIM reference [14] [15]. With the digital control module, the quadrature oscillator using CCII is shown in Fig 4. Where  $R_1=R_4/K_1$  and  $R_3=R_5K_1$

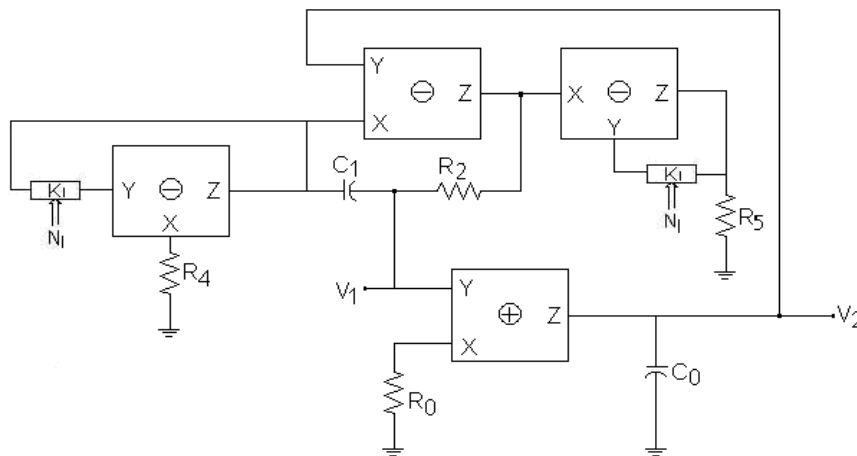


Fig. 4: DPQO with digital control word  $N_1$

This results in characteristic equation as

$$s^2 + s \left( \frac{1}{R_2 C_1} - \frac{1}{R_0 C_0} \right) + \left( \frac{\frac{R_5 K_1}{R_4 / K_1}}{R_0 C_0 R_2 C_1} \right) = 0 \quad (8)$$

condition of oscillation:  $C_0 R_0 = R_2 C_1$

Frequency of oscillation is

$$\omega_0 = \left( \frac{R_5 K_1^2 / R_4}{R_0 C_0 R_2 C_1} \right)^{\frac{1}{2}} \quad (9)$$

$R_0 = R_2 = R_4 = R_5 = R$  and  $C_0 = C_1 = C$

$$\omega_0 = \frac{N}{2^n RC} \quad (10)$$

It is to be noted that the frequency of oscillation  $\omega_0$  can be tuned over a wide range by controlling the digital control  $N_1$

### Case II: Digitally Programmable Quadrature Oscillator 2 (DPQO2)

For realizing DPQO2 the grounded resistor  $R_1$  is replaced by DPIM reference [14] having  $K_1$  – block where as  $R_3$  is replaced by DPIM having  $K_2$  – block, shown in Figure 5. Where  $R_1 = R_4 K_1$  and  $R_3 = R_5 K_2$

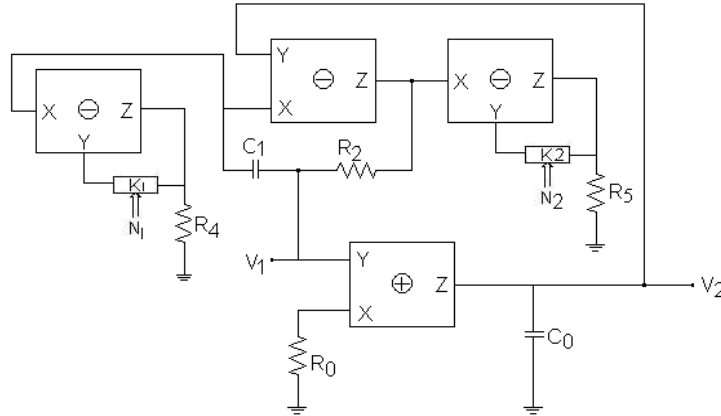


Fig. 5: DPQO with digital control word  $N_1$  and  $N_2$ .

This results in characteristic equation as

$$s^2 + s \left( \frac{1}{R_2 C_1} - \frac{1}{R_0 C_0} \right) + \left( \frac{\frac{R_5 K_2}{R_4 K_1}}{R_0 C_0 R_2 C_1} \right) = 0 \quad (11)$$

Condition of oscillation:  $C_0 R_0 = R_2 C_1$

$$\omega_0 = \left( \frac{R_5 K_2 / R_4 K_1}{R_0 C_0 R_2 C_1} \right)^{\frac{1}{2}} \quad (12)$$

If  $R_0 = R_2 = R_4 = R_5 = R$  and  $C_0 = C_1 = C$

$$\omega_0 = \frac{1}{RC} \left( \frac{N_2}{N_1} \right)^{\frac{1}{2}} \quad (13)$$

From equation (13), it is clear that the frequency of oscillation can be controlled directly through the digital control word  $N_2$  and inversely through digital control word  $N_1$ .

Hence in both the cases, the realized digitally programmable quadrature oscillators, frequency of oscillation can be controlled digitally by varying digital control word N.

## VI. SENSITIVITY STUDY

The incremental sensitivities for parameters used in digitally programmable quadrature oscillator given in equation (1) have been analysed and given as

$$\left| S_{R_0, R_1, R_2, C_0, C_1}^{\omega_0} \right| = \frac{1}{2} \quad (14a)$$

For equation (7) i.e. DPQO1 the sensitivity study is

$$\left| S_{R, C, K_1}^{\omega_0} \right| = 1 \quad (14b)$$

And the sensitivity study for equation (8) i.e. DPQO2 is

$$\left| S_{R, C}^{\omega_0} \right| = 1 \quad \left| S_{K_1, K_2}^{\omega_0} \right| = 1 \quad (14c)$$

The sensitivity of frequency of oscillation to passive and active components is quite low.

## VII. SIMULATION RESULTS

Tunable quadrature oscillator of Figure 1 was designed for a cut off frequency  $f_0 = 3\text{kHz}$  with  $C = 0.01 \mu\text{F}$  and  $R = 5.3 \text{ k}\Omega$ . The simulated response of this tunable quadrature oscillator is shown in Figure 6. The DPQO1 of Figure 4 having  $K_1$  block was designed for cut off frequency  $f_0 = 2.8125 \text{ KHz}$  with  $N=15$ ,  $C = 0.01 \mu\text{F}$  and  $R = 5.3 \text{ k}\Omega$ . Its simulated response is shown in Figure 7(a). The frequency variation with digital control word N is shown in Figure 7(b). The second case i.e. DPQO2 of Figure 5 having two K-block was designed for the cut off frequency  $f_0 = 3(N_2/N_1)^{1/2} \text{ KHz}$  with  $C = 0.01 \mu\text{F}$  and  $R = 5.3 \text{ K}\Omega$ . The simulated response is shown in Figure 8(a). The variation of frequency with digital control words  $N_1$  and  $N_2$  are shown in Figure 8(b). Also the frequency variation with  $R_4$  and  $R_1$  is also shown in Figure 8(c) and 8(d) respectively.

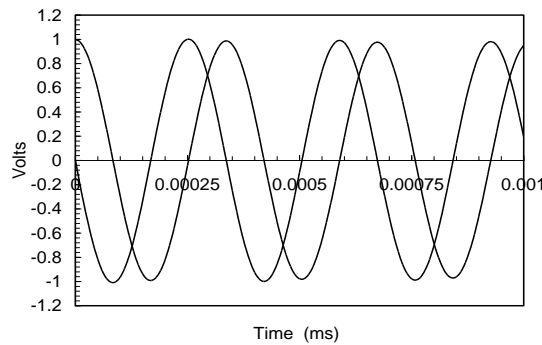


Fig. 6: Response for tunable quadrature oscillator.

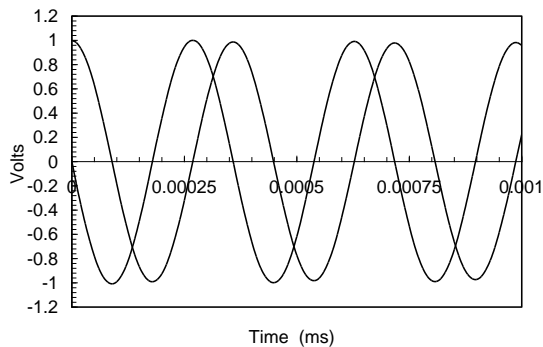


Fig. 7(a): Response for DPQO1 control

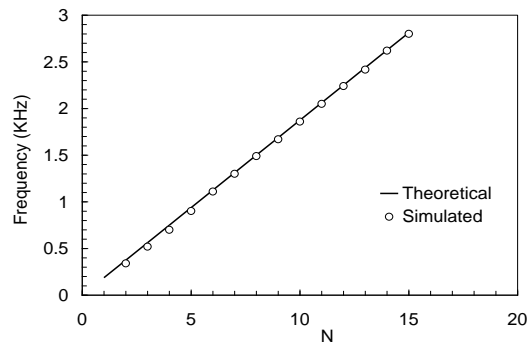


Fig. 7(b): Frequency variation of DPQO1 with digital Word  $N_1$

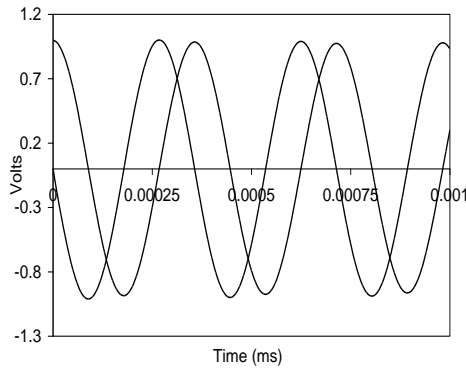


Fig. 8(a): Response for DPQO2.

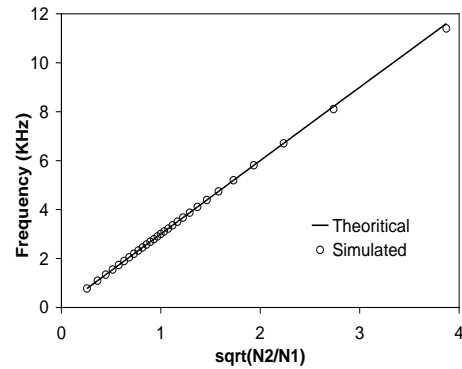


Fig. 8(b): Frequency variation of DPQO2 with digital Control word  $N_1$  and  $N_2$

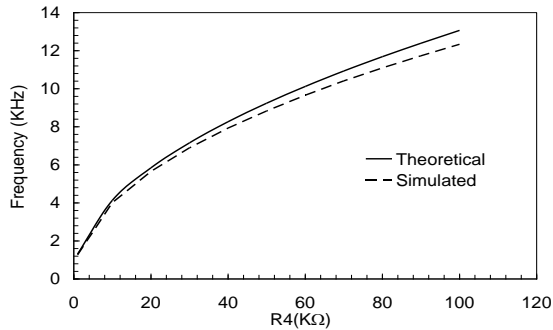


Fig. 8(c): Frequency variation of DPQO2 with  $R_4$

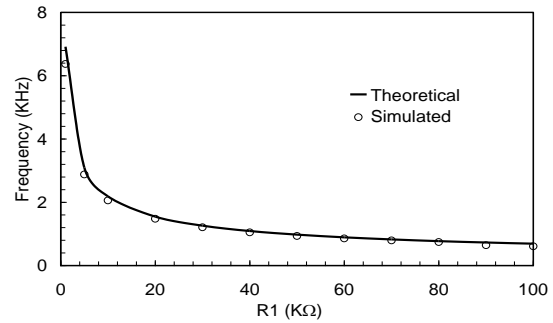


Fig. 8(d): Frequency variation of DPQO2 with  $R_1$

### VIII. CONCLUSION

A simple technique has been used to transform the tunable quadrature oscillator into a digitally programmable quadrature oscillator. The realized DPQOs exhibits quadrature outputs with equal magnitudes. The oscillator enjoys the attractive features of digital tuning of frequency of oscillation  $\omega_0$  through digital control words, low incremental sensitivities, large dynamic range, suitability for IC implementation and high resolution capability. The used digitally programmable circuit parameters are reconfigurable. The resolution of the digital control can be improved by using larger number of bits in the digital control module. All the realized circuits were designed and simulated using PSPICE. The results thus obtained verify the theory.

### REFERENCES

- [1]. A. S. Sedra and K.C Smith, "A second generation current conveyor and its applications," IEE Transactions on circuit theory, 1970, CT-17, pp. 132-134.
- [2]. B. Wilson, "Recent development in current conveyors and current mode circuits," IEE Proc. G,132, (2), 1990, pp. 63-67.
- [3]. I. A. Khan, M. R. Khan and N. Afzal, "Digitally programmable multifunctional filter using CCII's," J. of Active and Passive Devices." 2005, USA.
- [4]. M. T. Ahmed, I. A. Khan and N. Minhaj, "On transconductance – C quadrature oscillator," International Journal of Electronics, Vol. 83, pp. 201-207.
- [5]. Y. Sun, and J. F. Fidler, "Versatile active biquad based on second generation current conveyors," International Journal of Electronics, 1994, vol. 76, pp. 91-98.
- [6]. J. A. Svobodo, "Transfer function syntheses using current conveyors. International Journal of Electronics," 1994, 76, 611-614.
- [7]. I. A Khan and S. Khwaja, "An integrable gm-C quadrature oscillator. International Journal of Electronics," 2000 87(11), pp. 1353-7.
- [8]. Banlue Srisuchinwong, "Fully balanced current-tunable sinusoidal quadrature oscillator," Int.J.Electronics, Vol. 87, No. 5, 2000, pp. 547-556.
- [9]. S. I. Liu, "Single-resistance-controlled/voltage-controlled oscillator using current conveyors and grounded capacitors," Electron Letter, 31(5), 1995, pp. 337-8.

- [10]. Abuelma'atti and A. A. Ghumaiz, "Novel CCI – based single element controlled oscillators employing grounded resistors and capacitors," *IEEE Trans Circuits Syst-I: Fundamental Theory Application*, 43(2), 1996, pp. 153-5
- [11]. J. W. Horng, C. W. Chang, and M. H. Lee, "Single element controlled sinusoidal oscillators using CCII," *International Journal of Electronics*, 83(6), 1997, pp. 831-6
- [12]. J. W. Horng, C. L. Hou, C. M. Chang, W. Y. Chung, H. W. Tang, and Y. H. Wen, "Quadrature oscillator using CCII," *International Journal of Electronics*, Vol. 92, No. 1, 2006, pp. 21-31.
- [13]. I. A. Khan, and S Hasan, "Current mode four phase quadrature oscillator using CCII," *Journal of Active and Passive Electronic Devices*, Vol. 1, 2006, pp. 273-279.
- [14]. I. A. Khan, N. Afzal and M. R. Khan, "Digitally Programmable Generalized Impedance Multiplier Using CCI," *International Conference on Robotics, Vision, Information and Signal Processing, (ROVISP 2007)* 28<sup>th</sup> – 30<sup>th</sup> November 2007, Penang, Malaysia.
- [15]. I. A. Khan, N. Afzal and M. R. Khan., "A Digitally Programmable Impedance Multiplier using CCII with High Resolution Capability," *Journal of Active and Passive Electronic Devices*, 8, 2009, pp. 247-257.