

# Mathematical Model for Liquid Holdup in Multi Nozzle Jet Ejector

K S. Agrawal

Department of Petro Chemical Technology Polytechnic, The M. S. University of Baroda, Vadodara, Gujarat, India

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**Abstract:-** The dispersion of gases in liquids in many areas like chemical engineering, biochemical engineering and waste treatment systems is of prime importance. Hence, there have been many significant contributions in recent years in the development of more efficient gas- liquid ejector. In this paper we have made an attempt to develop a mathematical model for liquid hold up.

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## I. INTRODUCTION

Because of high energy efficiency in gas dispersion, many researchers used jet ejector and considerable amount of work has been done: (Jackson, 1964; Volmuller and Walburg, 1973; Nagel et al., 1970; Hirner and Blenke, 1977; Zehner, 1975; Pal et al., 1980; Ziegler et al., 1977).

It is important to note that the kinetic energy of a high velocity liquid jet is used for getting fine dispersion and mixing between the phases in the given gas liquid ejector. The studies in this area are listed below:

- (Zlokamik, 1980) has reported that oxygen absorption efficiency is as high as 3.8 kg O<sub>2</sub>/kwh in ejectors as compared to 0.8 kg O<sub>2</sub>/kwh in a propeller mixer. The higher gas dispersion efficiency of the ejector type can be understood from the well known fact : “gas dispersion is possible only if the fraction of micro turbulence is high” (Schugerl, 1982).
- Radhakrishnan et al. (1984) have used a vertical column fitted with a multi jet ejector for gas-dispersion for studying the pressure drop, holdup and interfacial area.

### 1.1.1 Hold up

Yamashita and Inoue (1975), Koetsier et al. (1976) and Mandal et al. (2003 and 2004) reported the holdup characteristics with respect to gas flow rate in the jet ejector. At lower range of gas flow rate, gas hold up increases with increase in gas flow rate but at higher range of gas flow rates the increase in gas flow rate decreases the gas hold up or it remain constant depending on the height of liquid in the follow up column is high or low respectively. At lower gas flow rates small bubbles produced are in large number and at higher gas flow rate due to coalescence the bubbles of larger size are produced which lead to decrease in number of bubbles. Hills (1976) has reported that the holdup is not affected by liquid flow rate. Mandal et al. (2004) observed that for the same gas flow rate the increase in liquid flow rate decreases the gas hold up. The variables  $A_R$ ,  $n$ ,  $Re_{ls}$  and  $Re_{gs}$  affect the liquid holdup in a jet ejector.

Radhakrishnan et al. (1984) obtained following correlation by applying multi linear regressions analysis on their experimental data:

$$\chi_1 = 1 - \exp \left[ -38.176 A_R^{-0.06} n^{-0.06} Re_{ls}^{0.0002} Re_{gs}^{-0.55} \right] \quad (1.1.1)$$

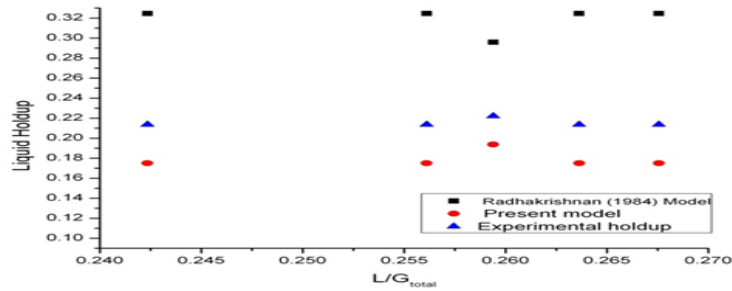
A new mathematical model has been attempted to predict the gas hold up as follows:

It is assumed that the model is of the form:

$$\alpha_1 = 1 - \exp \left[ a_1 A_R^b n^c Re_{ls}^d Re_{gs}^e \right]$$

Therefore  $\log[-\log(1 - \alpha_1)] = \log a_1 + b \log A_R + c \log n + d \log Re_{ls} + e \log Re_{gs}$ .

Using experimental data and multi linear regression analysis the values of  $a_1$ ,  $b$ ,  $c$ ,  $d$  and  $e$  were obtained. The values obtained are  $a_1 = -51.467$ ,  $b = -0.03$ ,  $c = 0.03$ ,  $d = 0.0002$  and  $e = -0.41$ .



**Figure 1.1.0 :** Comparison of liquid holdup predicted by Radhakrishnan (1984), present model and experimental value at different  $L/G_{total}$  ratio.

Thus mathematical model for gas hold up is as follows.

$$\alpha_1 = 1 - \exp \left[ -51.467 A_R^{-0.03} n^{-0.03} Re_{ls}^{0.0002} Re_{gs}^{-0.41} \right] \quad (1.1.2)$$

Liquid holdup may be determined by following equation.

$$\chi_1 = 1 - \alpha_1 = \exp \left[ -51.467 A_R^{-0.03} n^{-0.03} Re_{ls}^{0.0002} Re_{gs}^{-0.41} \right] \quad (1.1.3)$$

The results predicted from Radhakrishnan (1984) model and present model (equation – 1.1.3) is compared with actual experimental value at different  $L/G$  in figure (1.1.0).

#### Some Terminology

|                    |  |                   |
|--------------------|--|-------------------|
| $\chi_1$           | liquid holdup  | [-]               |
| $A_R$              | area ratio (ratio of cross section area of throat to nozzle) | [m <sup>2</sup> ] |
| $n$                | number of nozzles  | [-]               |
| $Re_{ls}, Re_{gs}$ | Reynold number based on superficial gas and liquid velocity  | [-]               |
| $\alpha_1$         | gas hold up  | [-]               |
| $a_1, b, c, d, e$  | constants  | [-]               |

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